



UNIVERSIDADE DA CORUÑA



Escola Politécnica Superior

Trabajo Fin de Máster
CURSO 2016/2017

BUQUE LNG DE MEMBRANA DE 145.000 m³

Máster en Ingeniería Naval y Oceánica

ALUMNA/O

Ismael Grandal Mouriz

TUTORAS/ES

Vicente Díaz Casas

FECHA

SEPTIEMBRE DE 2017

CUADERNO 1

En este cuaderno realizaremos un dimensionamiento preliminar del buque estudiando diferentes alternativas y seleccionando la más favorable y económica respecto a nuestras características.



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CURSO 2016/2017**

BUQUE LNG DE MEMBRANA DE 145.000 m³

Máster en Ingeniería Naval y Oceánica

CUADERNO 1

**ELECCIÓN DE LA CIFRA DE MÉRITO Y DEFINICIÓN DE ALTERNATIVAS.
SELECCIÓN DE LA MÁS FAVORABLE**

DEPARTAMENTO DE INGENIERÍA NAVAL Y OCEÁNICA
TRABAJO FIN DE MÁSTER
CURSO 2016-2017

PROYECTO NÚMERO: 17-32 P

TIPO DE BUQUE: Buque tanque LNG de membrana

CLASIFICACIÓN, COTA Y REGLAMENTOS DE APLICACIÓN: DNV, SOLAS, MARPOL, CIG.

CARACTERÍSTICAS DE LA CARGA: gas natural licuado con capacidad para 145.000 m³.

VELOCIDAD Y AUTONOMÍA: 19,5 nudos a la velocidad de servicio, 85% MCR + 15% MM. 12.000 millas a la velocidad de servicio.

SISTEMAS Y EQUIPOS DE CARGA / DESCARGA: los habituales en este tipo de buque.

PROPULSIÓN: Propulsión Diesel eléctrico. Dos líneas de ejes

TRIPULACIÓN Y PASAJE: 35 tripulantes en camarotes individuales.

OTROS EQUIPOS E INSTALACIONES: Las habituales en este tipo de buque.

Ferrol, Abril de 2017

ALUMNO: D. Ismael Grandal Mouriz

ÍNDICE:

1. INTRODUCCIÓN. GAS NATURAL Y BUQUES GASEROS.....	6
2. BASE DE DATOS.....	15
3. CÁLCULO DE LA ESLORA (Lpp).....	16
4. CÁLCULO DE LA MANGA (B).....	17
5. CÁLCULO DEL PUNTAL (D).....	18
6. CÁLCULO DEL CALADO (T).....	20
7. CÁLCULO DE LA RELACIÓN VOLUMEN/LBD.....	22
8. RESULTADOS DEL PRIMER DIMENSIONAMIENTO.....	23
9. CÁLCULO DE COEFICIENTES.....	23
10. ELECCIÓN DE LA CIFRA DE MÉRITO.....	26
11. CÁLCULO DEL PESO EN ROSCA.....	27
12. COSTES.....	29
13. ALTERNATIVA MÁS FAVORABLE.....	30
14. NUEVO CÁLCULO DE COEFICIENTES.....	32
15. ESTIMACIÓN DE LA POTENCIA.....	34
16. NUEVO CÁLCULO DEL PESO EN ROSCA, PESO MUERTO, DESPLAZAMIENTO Y CONSUMOS.....	36
17. CÁLCULO DEL FRANCOBORDO.....	38
18. ESPECIFICACIÓN PRELIMINAR.....	39
19. BIBLIOGRAFÍA.....	43

ANEXO I: INFORME DE LA HERRAMIENTA SOLVER

ANEXO II: BUQUES DE LA BASE DE DATOS

ANEXO III: CROQUIS CONCEPTUAL BUQUE PROYECTO

1-INTRODUCCIÓN. GAS NATURAL Y BUQUES GASEROS

Definición

El gas natural es una fuente de energía no renovable de origen fósil, que se encuentra normalmente en el subsuelo continental o marino. Se formó hace millones de años cuando una serie de organismos descompuestos, como animales y plantas, quedaron sepultados bajo lodo y arena, en lo más profundo de los antiguos lagos y océanos. En la medida que se acumulaba lodo, arena y sedimento, se fueron formando capas de roca a gran profundidad. La presión causada por el peso sobre estas capas más el calor de la Tierra, transformaron lentamente el material orgánico en petróleo crudo y gas natural.

El gas natural se acumula en bolsas entre la porosidad de las rocas subterráneas. Pero en ocasiones, se queda atrapado debajo de la tierra por rocas sólidas que evitan que el gas fluya, formándose lo que se conoce como un yacimiento.

La composición del gas natural incluye diversos hidrocarburos gaseosos, con predominio del metano (sobre el 90%), y en proporciones menores etano, propano, butano, pentano y pequeñas proporciones de gases inertes como dióxido de carbono y nitrógeno.

Es una de las fuentes de energía más limpias y respetuosas con el medio ambiente, ya que contiene menos dióxido de carbono y lanza menos emisiones a la atmósfera. Es, además, una energía económica y eficaz. Una alternativa segura y versátil capaz de satisfacer la demanda energética en los sectores doméstico, comercial e industrial.

El transporte de gas natural licuado

Realizaremos primeramente una pequeña introducción acerca del transporte de gas licuado desde diferentes perspectivas con la finalidad de familiarizarnos con este tipo de buques.

Se denomina LNG al gas natural que ha sido refrigerado por enfriamiento a aproximadamente $-160\text{ }^{\circ}\text{C}$.

El hecho de que el gas natural ocupe un volumen 600 veces menor licuado que en estado gaseoso, hace muy práctico su transporte en buques.

Se tratará la cadena de proceso de LNG, su evolución y demanda mundial y los diferentes tipos de buques destinados a su transporte.

Cadena integrada del proceso del LNG

Existen cuatro procesos principales que componen la cadena integrada del LNG:

Exploración y explotación del LNG

Comprende todas las operaciones relacionadas desde las reservas hasta las plantas de LNG.

Plantas de LNG

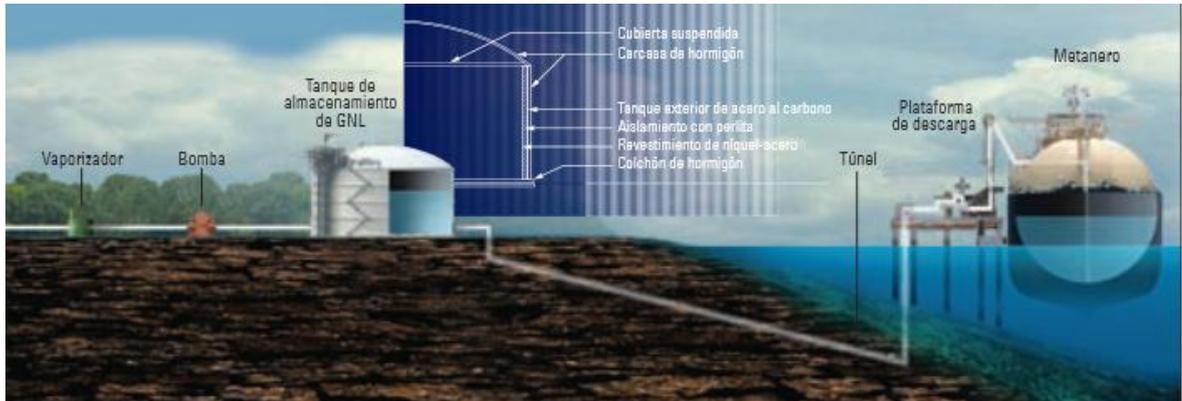
Incluye el tratamiento del gas natural, la licuefacción propiamente dicha y el almacenamiento de LNG.

Transporte

El transporte en buques metaneros es el tercer eslabón de la cadena integrada del LNG. Estos buques son menos contaminantes que otros medios de transporte, ya que pueden quemar gas natural en lugar de fuel oil como fuente de propulsión.

Terminales de recepción

Incluye la descarga, el almacenamiento, la regasificación y la distribución. El último eslabón de la cadena de suministro de LNG es la terminal de importación. Estas terminales descargan LNG y lo almacenan en tanques aislados hasta que esté preparado para ser sometido al proceso de regasificación.



Componentes de una terminal de importación. Los buques metaneros llegan por transporte marino a las plataformas de descarga de las terminales de importación, en tierra firme o en áreas marinas. Si las instalaciones de atraque y la plataforma de descarga asociada son marinas, el LNG proveniente de la embarcación se bombea a través de tuberías submarinas hasta los tanques de almacenamiento aislados, emplazados en tierra firme. Los tanques de acero aislados se utilizan comúnmente con fines de almacenamiento.

En la figura se muestra un esquema simplificado de dicha cadena:



Evolución de la demanda mundial de LNG

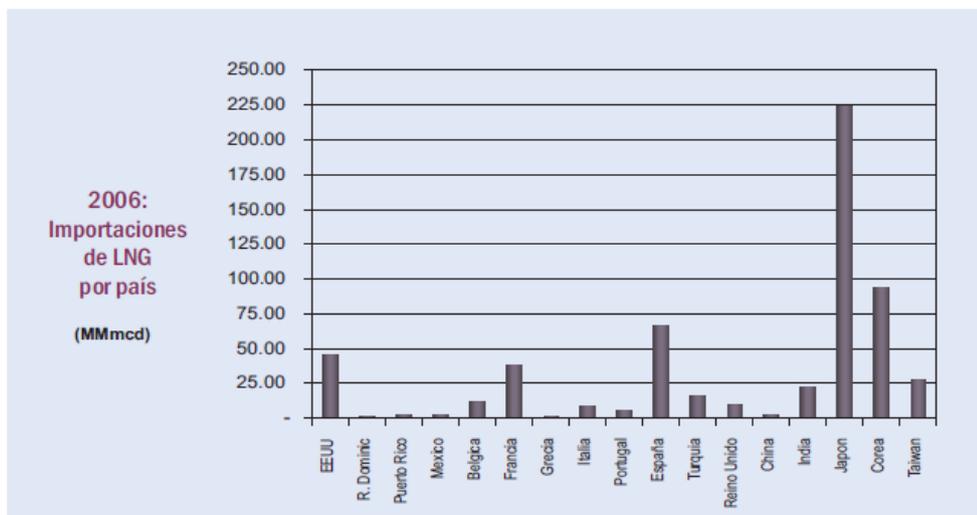
El LNG es un mercado en alza debido sobre todo a la explotación de bolsas de gas en zonas de perforación en las que previamente han agotado sus reservas de petróleo. La aparición de economías emergentes, como China o La India, han provocado un incremento continuado de la demanda de gas natural licuado.

La comercialización del gas licuado está concentrándose mayoritariamente en Asia. Solamente Japón representa el 52% del total de importaciones por barco.

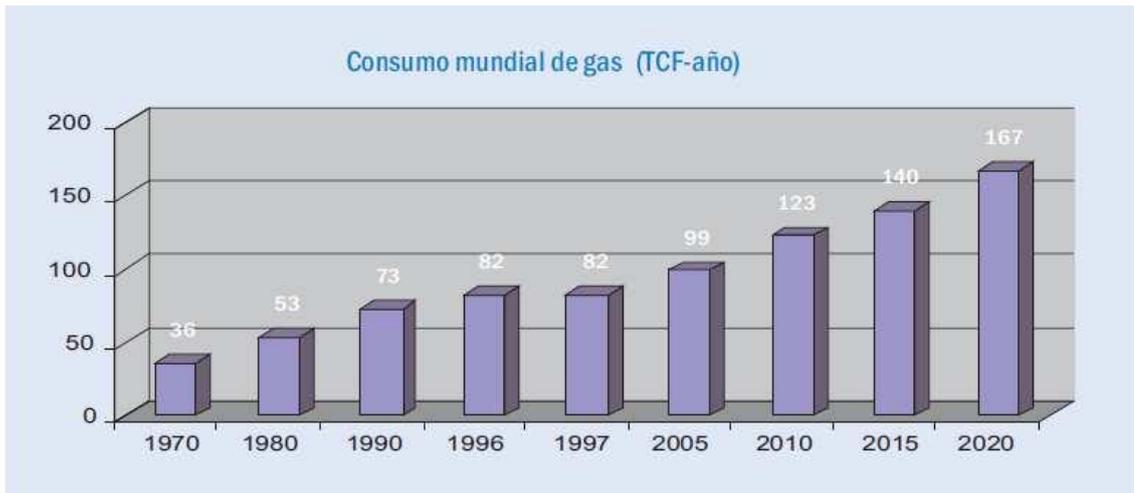
En el gráfico adjunto podemos observar las principales rutas de transporte del gas natural licuado:



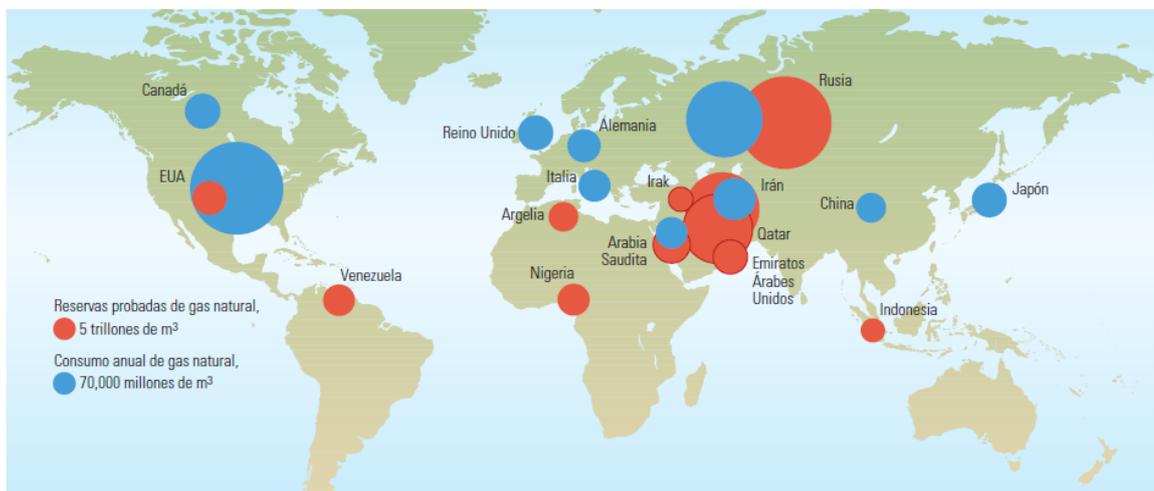
En la gráfica adjunta podemos ver las importaciones por países:



En la figura puede observarse el crecimiento histórico hasta el año 2010 de la demanda mundial de LNG, y su correspondiente pronóstico hasta el 2020. Como vemos, las previsiones son halagüeñas, aunque deberá tenerse en cuenta la crisis financiera que se vive en la actualidad, que previsiblemente rebajará estas estimaciones.



Reservas mundiales



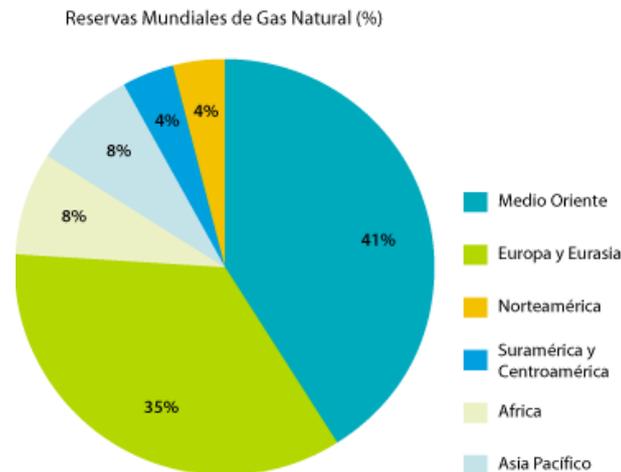
La búsqueda de gas natural se inicia con exploraciones, que consisten básicamente en realizar perforaciones en zonas donde existen indicios de la existencia de gas. Una vez que se encuentra un yacimiento de gas natural, el próximo paso es analizarlo para determinar tanto la cantidad como la calidad del gas natural contenido en ese yacimiento, calculándose así la duración de explotación del mismo de acuerdo a la cantidad de gas que contenga y a una estimación del consumo. Una vez que estos análisis son efectuados, el gas natural de ese yacimiento pasa a ser una “reserva probada” de gas natural.

Pero, dado el alto costo que implica este proceso, no todos los yacimientos son analizados. Lo que sí se realiza constantemente son perforaciones para localizar yacimientos, de manera que en el momento que se necesiten probar las reservas, éstas se tengan ubicadas y lo único necesario por realizar sea un análisis para determinar la calidad y la duración del gas natural.

Como norma, las empresas productoras de gas natural deben mantener reservas probadas por lo menos para cumplir con los contratos de extracción y suministro que mantenga vigentes.

Respecto a las reservas mundiales de gas natural, éstas son aproximadamente de 145 trillones de metros cúbicos. Estas reservas están localizadas principalmente en la ex Unión Soviética y Oriente Medio. Y dentro de la ex Unión Soviética, Rusia tiene el

85% de esas reservas. En el caso de Oriente Medio, Irán es el país que tiene mayor cantidad de reservas, con un 47%.



Proceso de licuefacción en tierra

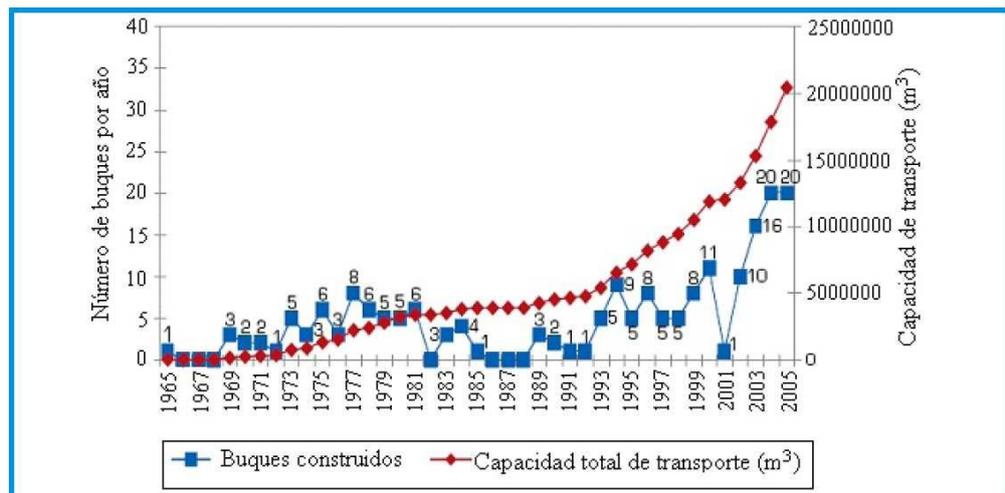
El LNG ocupa aproximadamente 600 veces menos volumen que el gas natural, gracias al proceso de licuefacción al que es sometido

El proceso de licuefacción tiene un rendimiento del 90%. Esto quiere decir que el 10% del gas natural que ingresa a la planta de LNG, se utiliza como fuente de energía para el proceso.

Se almacena en tanques criogénicos de 100.000 m³ de capacidad, que permiten mantener el gas en su forma líquida, aún en un clima cálido.

Evolución de los buques metaneros en el mundo

En esta figura se observa la evolución de la flota metanera en el mundo, desde 1965 hasta el 2006.



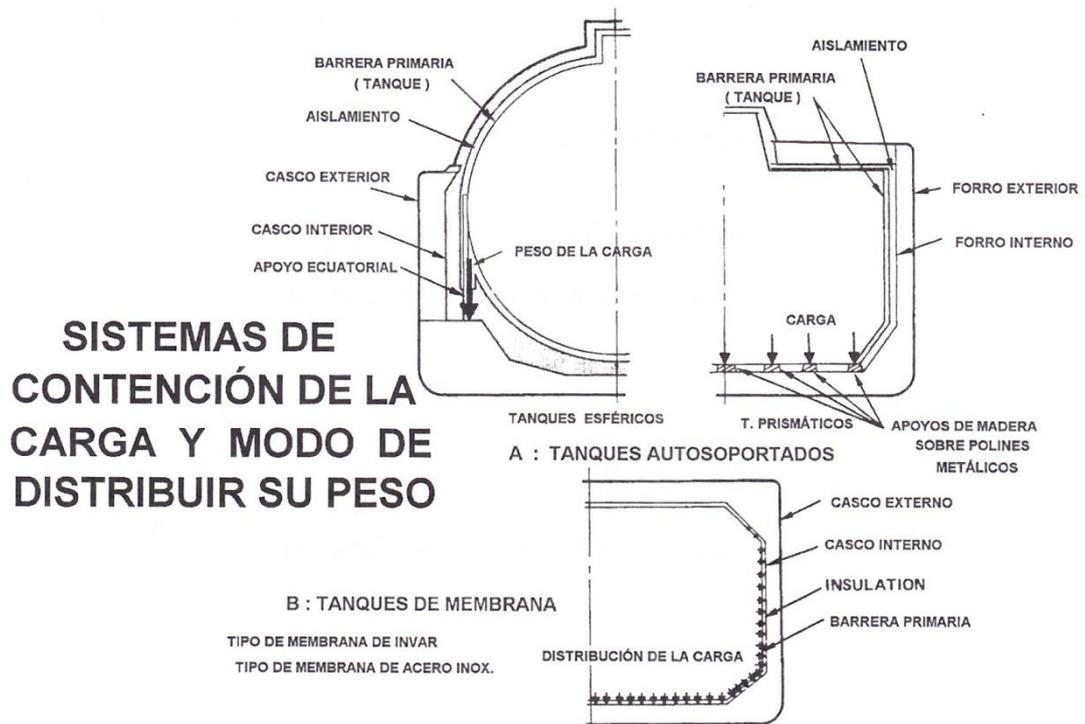
En el mundo, son 8 las empresas principales que construyen los buques metaneros, de las cuales 3 está en Japón, 3 en Corea y las otras 2 en Europa. Sin embargo, La India, China y Polonia están en condiciones tecnológicas para unirse a este grupo de constructores, al igual que sucede con otros países.

España parece haber cerrado su etapa en la construcción de buques metaneros con la desmantelación de los almacenes que se construyeron para la catalogación y almacenaje de las cajas de perlita.

Diferentes tipos de buques para el transporte de gas

Estos tipos de buques transportan gas licuado a la presión atmosférica y a una temperatura de -161 ° C.

El gas metano o “gas grisú” de las minas, o gas de los pantanos, es extremadamente peligroso por el riesgo de explosión. Esto obliga a que este tipo de buques incorporen grandes medidas de seguridad. Puede afirmarse que en el momento actual es el buque mercante de más alta tecnología.



Desde el punto de vista del sistema de contención de la carga, pueden distinguirse dos tipos diferentes:

- Los metaneros de tanques autoportados.
- Los metaneros de membrana.

Dentro de los metaneros de tanques independientes existen dos tipos de tecnología diferentes:

- La de General Dynamics, de tanques autoportados prismáticos (patente EEUU).
- La de Moss Rosenberg, de tanques autoportados esféricos (patente Dinamarca).

En ambos casos el material de los tanques es aluminio aleado (5083).

Los tanques autoportados de forma prismática se apoyan sobre polines de acero aleado (9% Ni) que van soldados al doble fondo. Los tanques sufrirán grandes dilataciones a causa del gran salto térmico de aproximadamente 200 ° C, a pesar del

bajo coeficiente de dilatación del aluminio. Ello obliga a que el sistema de contención de la carga permita las libres dilataciones sin ofrecer resistencia, pero sin dejar de tener sujeto al tanque. Esto se logra por un sistema de llaves en cruz situadas en el fondo (transversal y longitudinal) que dejan expandir o contraer libremente al tanque hacia proa y popa de la línea de llaves, pero al mismo tiempo impidiendo el libre movimiento del tanque respecto del buque. En dirección vertical también es preciso contar con unas guías sobre los mamparos de proa y popa que permitan la expansión o contradicción del tanque en sentido vertical, pero sin dejar a este libre respecto del buque. La sección del tanque es octogonal, sobresaliendo su parte alta sobre la cubierta, la cual se cubre con una cubierta tronco con el fin de evitar el impacto de los rayos solares sobre el mismo tanque, lo que aumentaría la evaporación y mayores pérdidas del gas durante el transporte (12oil-off).

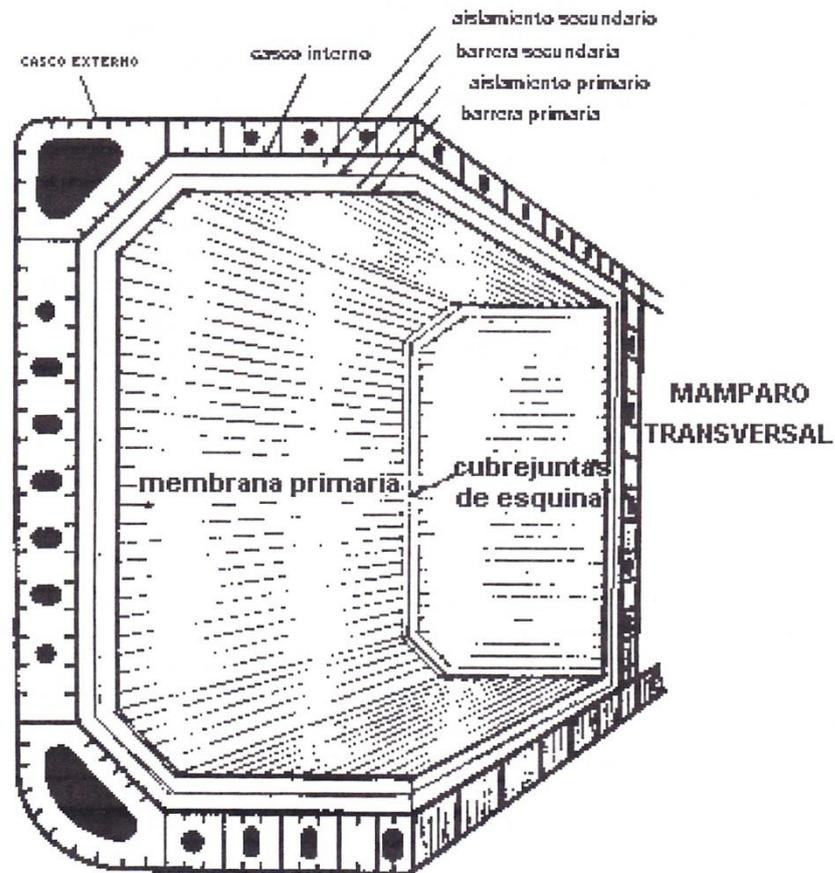
Los metaneros de tanques autosoportados esféricos, dan apoyo a las esferas contenedoras de la carga con anillos estructurales ecuatoriales, como se puede ver en la FIGURA. Produciéndose la libre dilatación del tanque en dirección a sus polos. Hace pocos años se hizo algún intento de fabricar el contenedor esférico con acero aleado al 9 % Ni, pero resultó un procedimiento inefectivo, a causa de las incontrolables tensiones térmicas que aparecían en sus soldaduras, las cuales provocaban grietas, fisuras y deformaciones.

La membrana es una lámina delgada que se apoya en toda su superficie en las cajas de madera que contienen el aislamiento. Coexisten dos tecnologías en las membranas de metaneros:

- Membrana de INVAR de acero aleado al 36 % Ni con bajísimo coeficiente de dilatación, su espesor es de 0.4 mm. Tecnología francesa de la firma Gaz Transport. (Ver figura).

- Membrana corrugada de acero inoxidable de 2/3 mm de espesor. Las corrugas se disponen perpendicularmente para poder absorber las libres dilataciones. Las zonas planas entre corrugas son las únicas que están apoyadas sobre las cajas de aislamiento. También es de tecnología francesa, de la firma Technigaz, en la actualidad fusionada con Gaz Transport.

TÉCNICA DE MEMBRANA DE GAZ-TRANSPORT DE INVAR (36 % Ni)



Los buques para el transporte de Gas Natural Licuado (GNL o LNG), tienen una ventaja muy importante desde el punto de vista de contaminación atmosférica: queman el propio gas natural en lugar de fuel oil como fuente de propulsión, con la consiguiente reducción de emisiones (aproximadamente un 90 %), altamente contribuyentes al efecto invernadero.

Además, dentro de los distintos tipos, podemos establecer las siguientes apreciaciones:

Los tanques de esferas tipo Moss tienen más superficie expuesta al viento, con lo que su resistencia al viento es elevada.

El precio de construcción de los buques con tanques esféricos es más elevado que el de los buques de membrana.

Los tanques prismáticos SPB presentan mayor manga en la parte superior del tanque, con lo que su momento por superficies libres es mayor que en los tanques

de membrana.

Los tanques de membrana ofrecen más capacidad de carga que los tanques esféricos.

En los tanques de membrana el enfriamiento de los mismos es más rápido que en los esféricos.



2-BASE DE DATOS

Hemos seleccionado una serie de buques transportadores de LNG con membranas con unas características similares a las de nuestro buque proyecto, con un volumen de carga en una franja que va desde los 138.000 hasta los 177.400 m³.

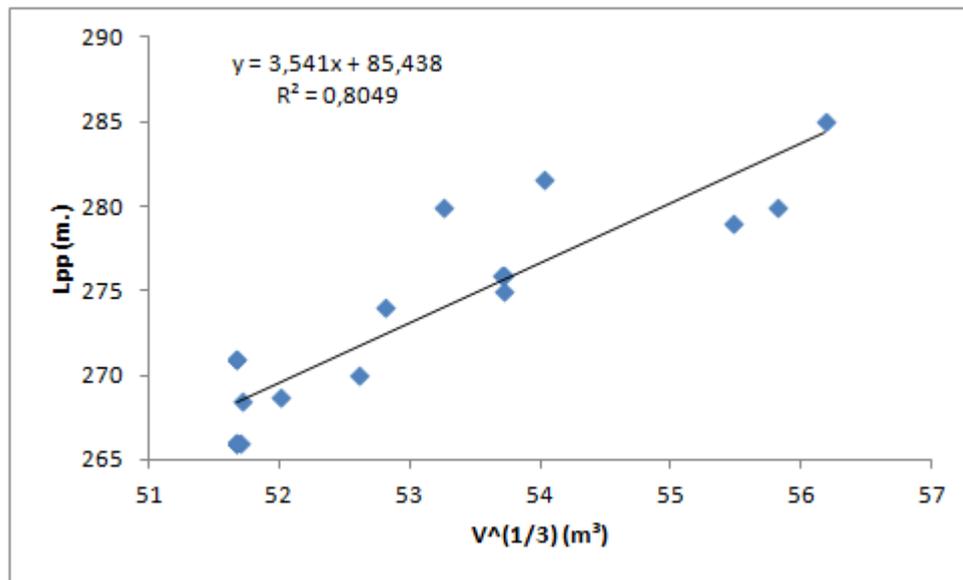
Toda la documentación correspondiente a los barcos que forman parte de la base de datos se adjunta como anexo.

Buque	V (m ³)	Lpp (m.)	B (m.)	D (m.)	T (m.)	v (kn.)
Abdelkader	17740 0	285	46	26,8	11,9	19,6
Castillo de Santisteban	17388 7	280	46	26	11,5	20,42
Barcelona Knutsen	17072 3	279	45,8	26,5	11,95	19,5
Seri Balhaf	15772 0	281,6	46,5	25,8	11,15	19,5
British Emerald	15500 0	275	44,2	26	11,47	20
Trinity Arrow	15498 2	276	44,7	26	11,37	19,5
GDF Suez Point Fortin	15491 3	276	44,7	26	11,73	19,5
Express	15100 0	280	43,4	26	11,6	19,2
Dapeng Sung	14733 7	274,1	43,35	26,25	11,45	19,5
Maersk Qatar	14560 0	270	43,4	26	11,4	20,6
Fernando Tapias	14062 7	268,8	43,4	26	11,42	19,5
Hanjin Muscat	13836 6	268,5	43	26,2	11,3	20,3
British Trader	13820 0	266	42,6	26	11,35	20,1
Excelsior	13800 0	266	43,4	26	11,5	19,1
Berge Everett	13800 0	266	43,4	26	11,4	19,5
SK Summit	13800 0	266	43,4	26	11,3	20,3
Sestao Knutsen	13800 0	271	42,5	25,4	11,4	19,5

	13800					
Iñigo Tapias	0	271	42,5	25,4	11,4	21

3-CÁLCULO DE LA ESLORA (Lpp)

En la gráfica posterior se representa la eslora y la raíz cúbica del volumen de los buques de carga de nuestra base de datos:



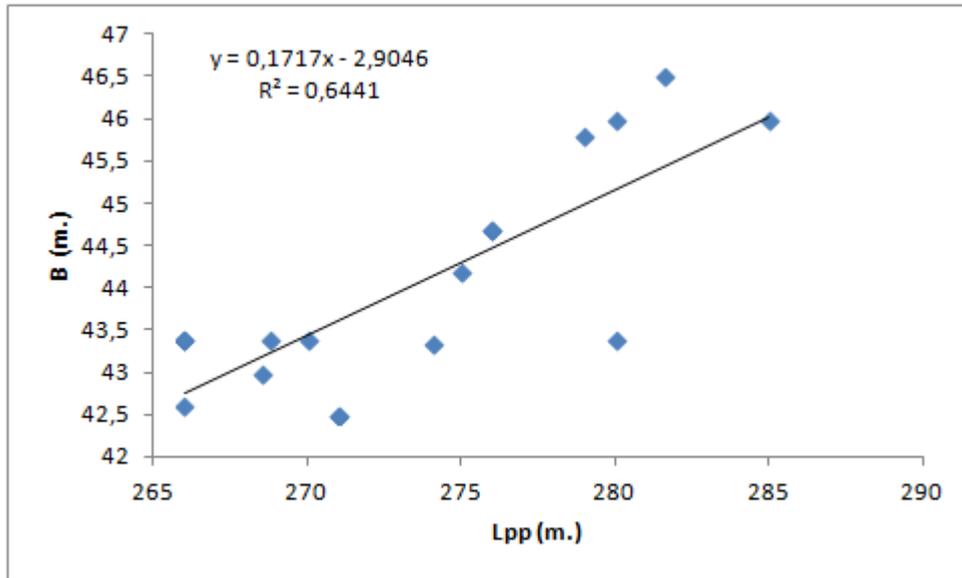
$$Lpp = 3,541 \cdot \sqrt[3]{V} + 85,438$$

$$\underline{Lpp = 271,5 \text{ m.}}$$

Donde:

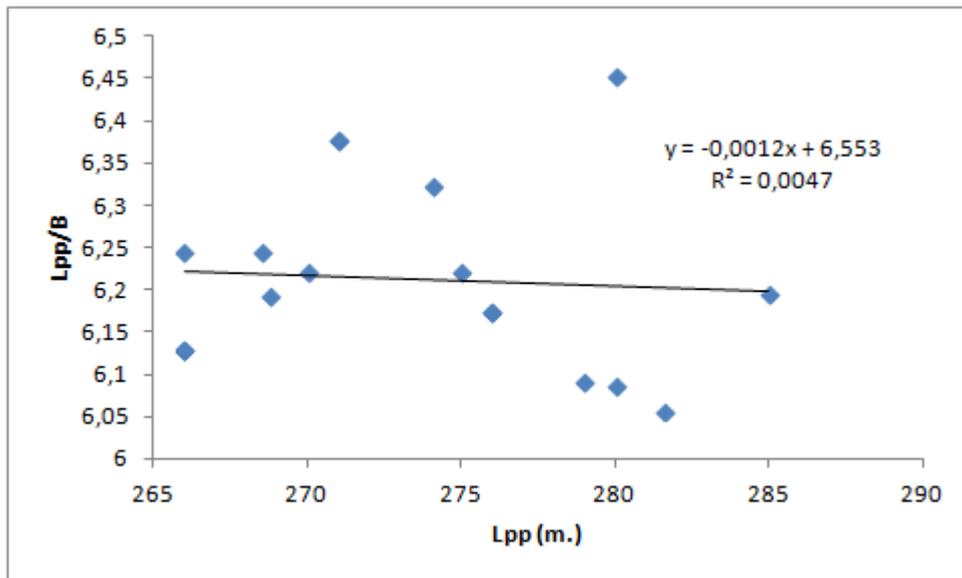
V: volumen de carga (145.000 m³)

4-CÁLCULO DE LA MANGA (B)



$$B = 0,1717 \cdot Lpp - 2,9046$$

$$B = 43,33 \text{ m.}$$



$$\frac{Lpp}{B} = -0,0012 \cdot Lpp + 6,553$$

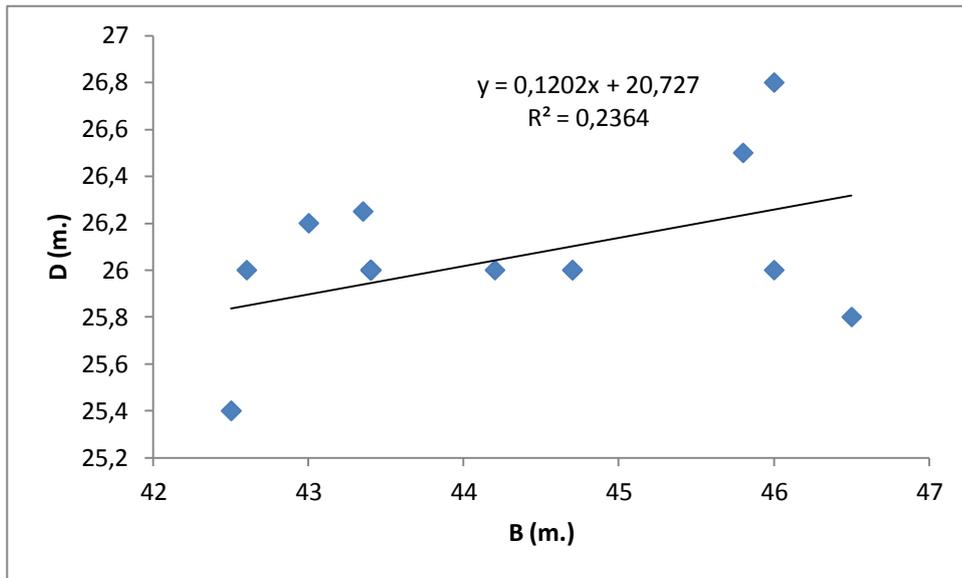
$$B = 43,22 \text{ m.}$$

Ésta no es una aproximación muy buena ($R^2 = 0,0047$), pero haremos una media de los dos valores obtenidos.

Hacemos una media de los dos valores anteriormente obtenidos de la manga (43,33 y 43,22) y tenemos como resultado 43,27, por tanto tomaremos una manga de:

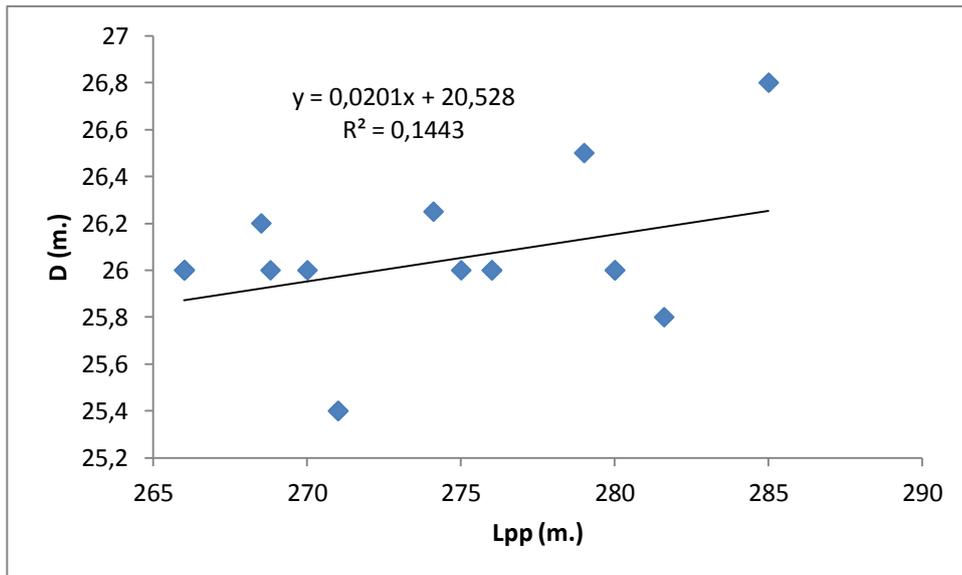
$$\underline{B = 43,30 \text{ m.}}$$

5-CÁLCULO DEL PUNTAL (D)



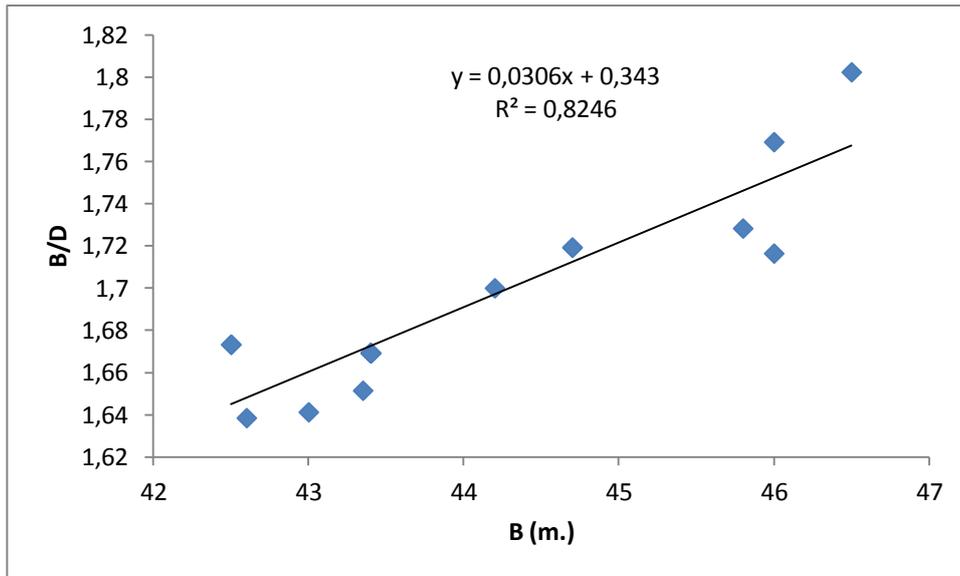
$$D = 0,1202 \cdot B + 20,727$$

$$D = 25,93 \text{ m.}$$



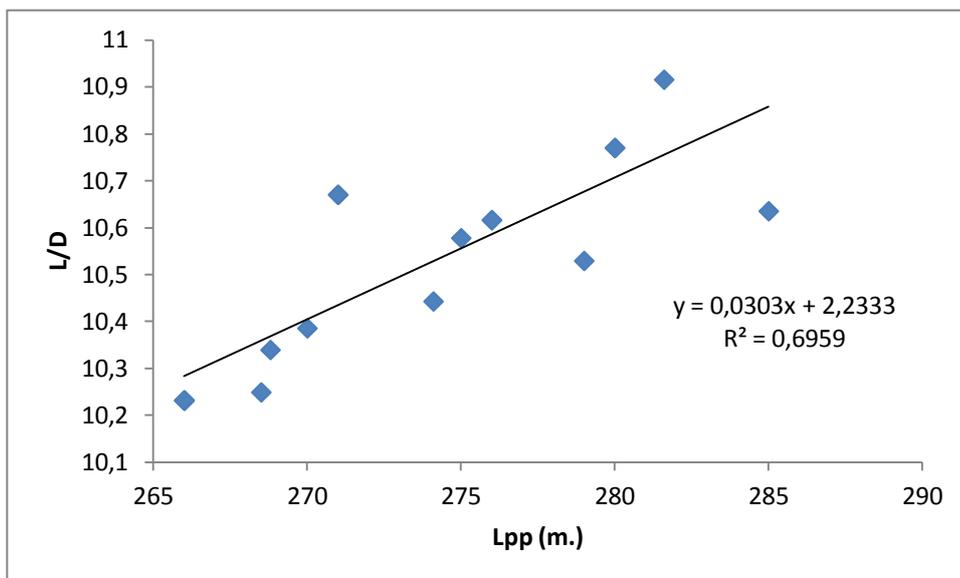
$$D = 0,0201 \cdot Lpp + 20,528$$

$$D = 25,94 \text{ m.}$$



$$\frac{B}{D} = 0,0306 \cdot B + 0,343$$

$$D = 25,96 \text{ m.}$$



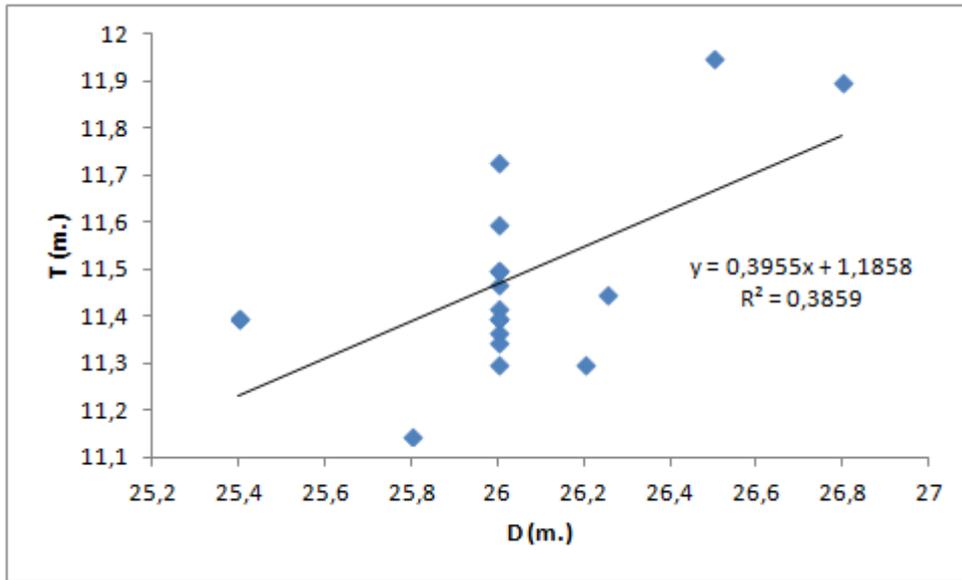
$$\frac{Lpp}{D} = 0,0303 \cdot Lpp + 2,2333$$

$$D = 25,91 \text{ m.}$$

Como en el caso de la manga, hay algunas aproximaciones que no son muy buenas, pero hacemos una media de los cuatro valores anteriormente obtenidos para el puntal (25,93; 25,94; 25,96 y 25,91) y tenemos como resultado 25,93. Por tanto, tomaremos un puntal de:

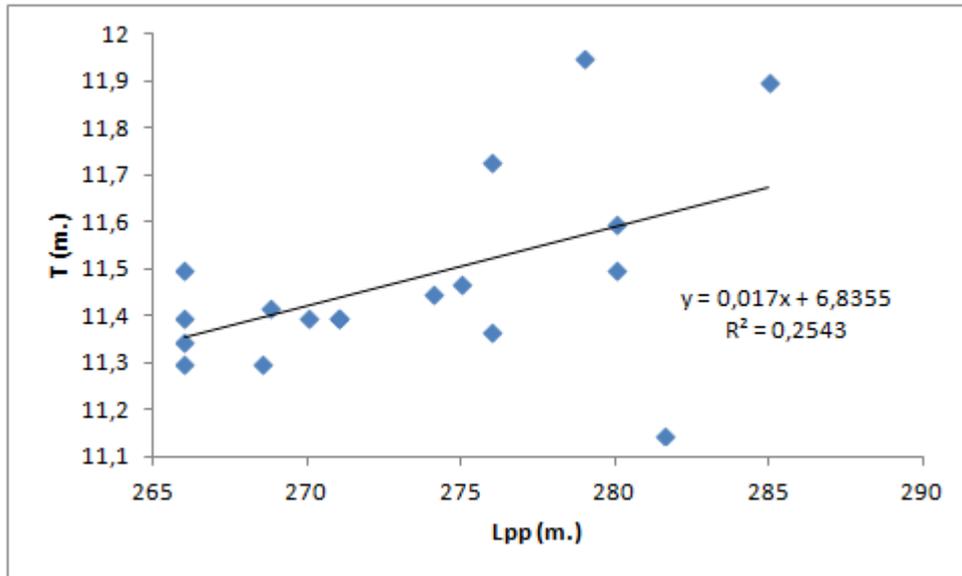
$$\underline{D = 26 \text{ m.}}$$

6-CÁLCULO DEL CALADO (T)



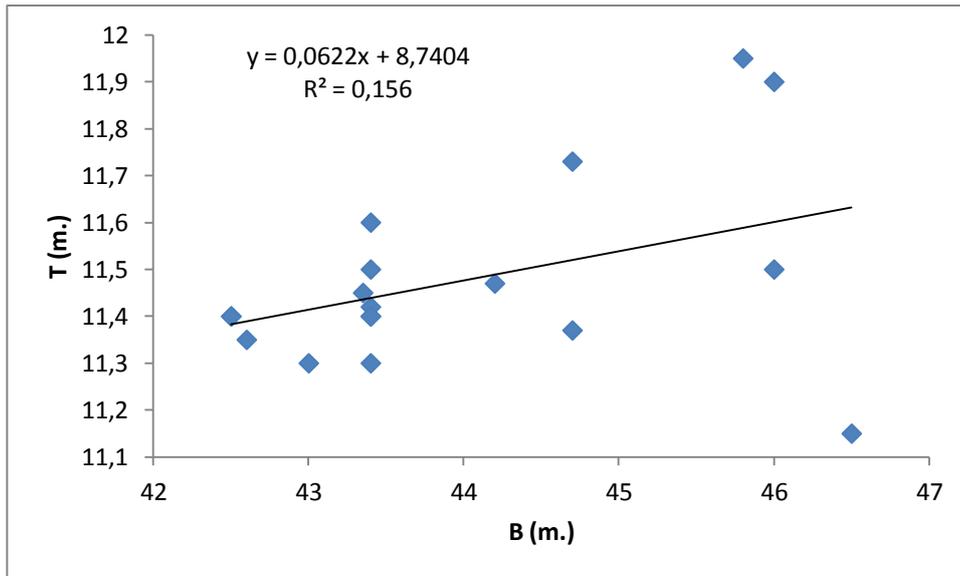
$$T = 0,3955 \cdot D + 1,1858$$

$$T = 11,47 \text{ m.}$$



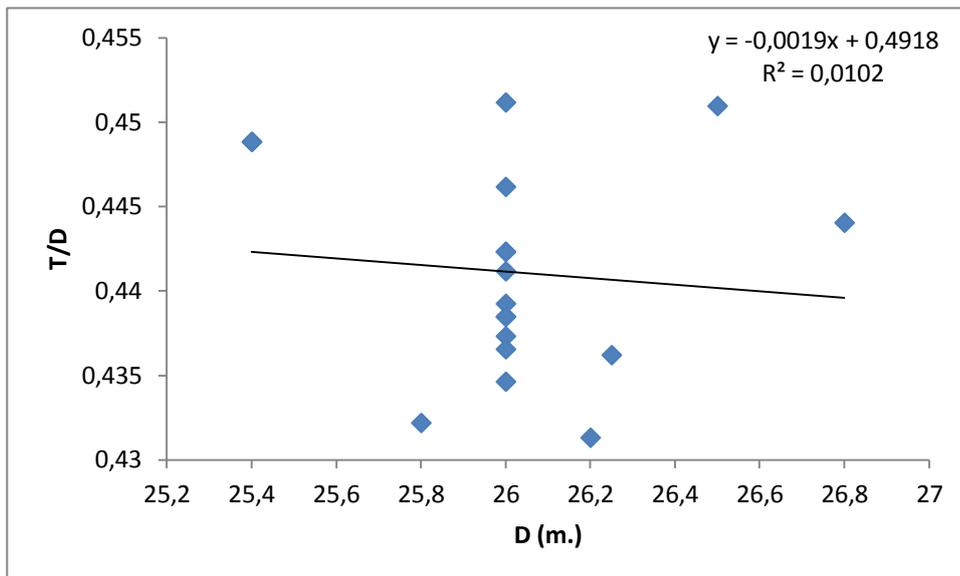
$$T = 0,017 \cdot Lpp + 6,8355$$

$$T = 11,41 \text{ m.}$$



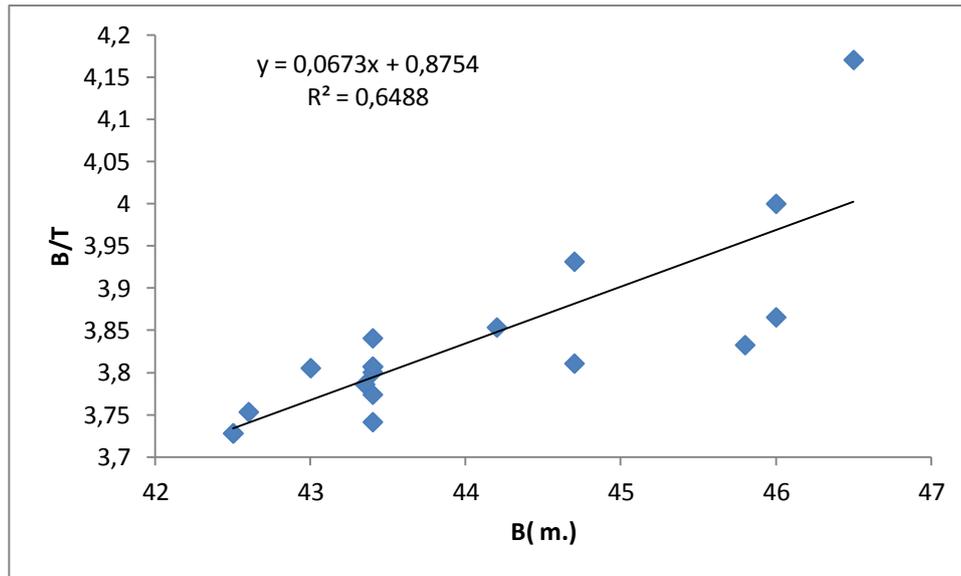
$$T = 0,0622 \cdot B + 8,7404$$

$$T = 11,43 \text{ m.}$$



$$\frac{T}{D} = -0,0019 \cdot D + 0,4918$$

$$T = 11,50 \text{ m.}$$



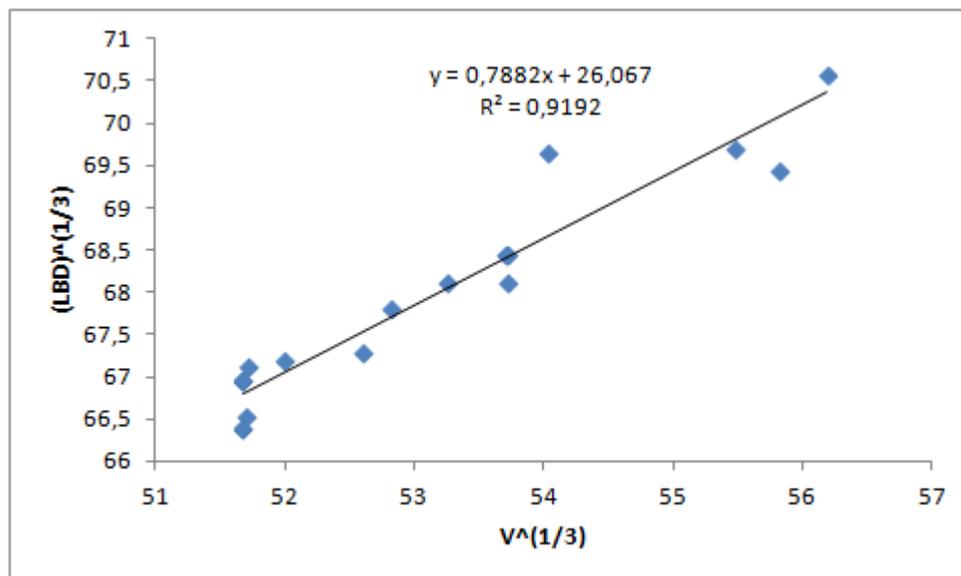
$$\frac{B}{T} = 0,0673 \cdot B + 0,8754$$

$$T = 11,43 \text{ m.}$$

Como en los dos casos anteriores, hay aproximaciones que no son muy buenas, pero las tendremos en cuenta a la hora de hacer una media de los cinco valores anteriormente obtenidos para el calado (11,47; 11,41; 11,43; 11,50 y 11,43). El valor medio es 11,45 m. Tomaremos un calado de:

$$T = 11,50 \text{ m.}$$

7-CÁLCULO DE LA RELACIÓN VOLUMEN/LBD



$$\sqrt[3]{LBD} = 0,7882 \cdot \sqrt[3]{V} + 26,067$$

Mediante esta fórmula calculamos nuestro LBD_{requerido} para transportar los 145.000 m³, que es igual a 307.215,93, y nuestro LBD es igual a 305.654,7. No se cumple la ecuación. Pero hay que tener en cuenta que en muchas de las gráficas estamos utilizando valores de R² de 0,50 o 0,60, por lo que hay un error de cálculo.

8-RESULTADOS DEL PRIMER DIMENSIONAMIENTO

L (m.)	B (m.)	D (m.)	T (m.)	LBD (m ³)
271,5	43,3	26	11,5	30721 5,93

9-CÁLCULO DE COEFICIENTES

Por tratarse de un barco de volumen utilizaremos las siguientes expresiones para la determinación de V_h (volumen del casco):

$$V_h = C_{BD} \cdot L \cdot B \cdot D$$

$$V_h = 265.675,06 \text{ m}^3$$

$$C_{BD} = C_B + C \cdot \frac{D-T}{T} (1 - C_B)$$

$$C_{BD} = 0,8692$$

Donde:

$C = 0,3$, para formas en U

Número de Froude

$$Fn = \frac{V}{\sqrt{g \cdot L}}$$

$$Fn = 0,1943$$

Donde:

V: velocidad de servicio (19,5 knot \approx 10,03 m/s)

g: aceleración de la gravedad (9,81 m/s²)

Lpp: eslora entre perpendiculares (271,5 m.)

Coefficiente de la maestra

$$C_m = 1 - 2 \cdot Fn^4$$

$$C_m = 0,9971$$

Coefficiente prismático

$$C_p = 1.2 - 2.1 \cdot Fn$$

$$C_p = 0,7920$$

Coeficiente de bloque

$$C_B = C_m \cdot C_p$$

$$\underline{C_B = 0,7897}$$

A continuación vamos utilizar otra serie de fórmulas para calcular el coeficiente de bloque

Alexander:

$$C_B = 1.08 - 1.68 \cdot Fn$$

$$\underline{C_B = 0,7535}$$

Van Lameren:

$$C_B = 1.137 - 2.02 \cdot Fn$$

$$\underline{C_B = 0,7445}$$

Ayre:

$$C_B = 1.05 - 1.68 \cdot Fn$$

$$\underline{C_B = 0,7235}$$

Minorsky:

$$C_B = 1.22 - 2.38 \cdot Fn$$

$$\underline{C_B = 0,7575}$$

Katsoulis:

$$C_B = 0.8217 \cdot f \cdot L^{0.42} \cdot B^{-0.3072} \cdot D^{0.1721} \cdot V^{-0.6135}$$

$$\underline{C_B = 0,7999}$$

Donde:

f: es un factor de corrección por tipo de buque. En el caso de un gasero toma el valor de 1,04.

Para finalizar, vamos a coger dos barcos de la base de datos de los que conocemos su desplazamiento. A partir de este valor podremos conocer su coeficiente de bloque y determinar las constantes a y b de la siguiente expresión:

$$C_B = a - b \cdot Fn$$

Tomamos como referencia los buques *Dapeng Sun* y *Maersk Qatar*.

C_B (Dapeng Sun) = 0,8191 y un desplazamiento de 114.789 t.

C_B (Maersk Qatar) = 0,7413 y un desplazamiento de 102.000 t.

Con el resto de datos de ambos buques sustituimos en las ecuaciones anteriores y obtenemos unos valores de a y b de:

$$a = 2,023$$

$$b = 6,224$$

Por tanto, para nuestro caso tendremos un $\underline{C_B = 0,8136}$

Haciendo una media de todos los valores obtenidos para el coeficiente de bloque: $C_B = 0,7688$. Y por tanto, como primera aproximación:

$$\Delta = C_B \cdot \rho \cdot L \cdot B \cdot T = 106.535,12 \approx 106.536 t.$$

Donde:

$$C_B = 0,7688$$

ρ : densidad del agua salada (1,025 t/m³)

$L \rightarrow L_{pp}$: eslora entre perpendiculares (271,5 m.)

B : manga de trazado (43,3 m.)

T : calado de diseño (11,5 m.)

Con los datos obtenidos anteriormente podemos hacer una nueva estimación de la eslora:

$$L = \left(\frac{V_h (L/B)^2 \cdot (B/D)}{C_{BD}} \right)^{1/3}$$

Donde:

V_h : Volumen del casco (265.675,06 m³)

$L \rightarrow L_{pp}$: eslora entre perpendiculares (271,5 m.)

B : manga de trazado (43,3 m.)

D : puntal a la cubierta principal (26 m.)

C_{BD} : coeficiente de bloque al 85%D (0,8692)

Tenemos como resultado $L = 271,49$ m., prácticamente el mismo valor que el obtenido por regresión lineal.

Las relaciones entre dimensiones de nuestra base de datos son:

Buque	L/B	B/D	B/T	L/D	T/D
Abdelkader	6,19 57	1,7 164	3,8 655	10,6 343	0,4 440
Castillo de Santisteban	6,08 70	1,7 692	4,0 000	10,7 692	0,4 423
Barcelona Knutsen	6,09 17	1,7 283	3,8 326	10,5 283	0,4 509
Seri Balhaf	6,05 59	1,8 023	4,1 704	10,9 147	0,4 322
British Emerald	6,22 17	1,7 000	3,8 535	10,5 769	0,4 412
Trinity Arrow	6,17 45	1,7 192	3,9 314	10,6 154	0,4 373
GDF Suez Point Fortin	6,17 45	1,7 192	3,8 107	10,6 154	0,4 512

Express	6,45 16	1,6 692	3,7 414	10,7 692	0,4 462
Dapeng Sung	6,32 30	1,6 514	3,7 860	10,4 419	0,4 362
Maersk Qatar	6,22 12	1,6 692	3,8 070	10,3 846	0,4 385
Fernando Tapias	6,19 35	1,6 692	3,8 004	10,3 385	0,4 392
Hanjin Muscat	6,24 42	1,6 412	3,8 053	10,2 481	0,4 313
British Trader	6,24 41	1,6 385	3,7 533	10,2 308	0,4 365
Excelsior	6,12 90	1,6 692	3,7 739	10,2 308	0,4 423
Berge Everett	6,12 90	1,6 692	3,8 070	10,2 308	0,4 385
SK Summit	6,12 90	1,6 692	3,8 407	10,2 308	0,4 346
Sestao Knutsen	6,37 65	1,6 732	3,7 281	10,6 693	0,4 488
Iñigo Tapias	6,37 65	1,6 732	3,7 281	10,6 693	0,4 488

A continuación se muestran los valores medios de estas relaciones y los intervalos máximo y mínimo en los que nos vamos a mover, que nos pueden ser de utilidad.

	L/B	B/D	B/T	L/D	T/D
MÁXIMO	6,45 16	1,8 023	4,1 704	10,9 147	0,4 512
MÍNIMO	6,05 59	1,6 385	3,7 281	10,2 308	0,4 313
VALOR MEDIO	6,21 21	1,6 915	3,8 353	10,5 055	0,4 411

10-ELECCIÓN DE LA CIFRA DE MÉRITO

Los criterios usados con más frecuencia son los siguientes:

- Coste de construcción mínimo
- Inversión total mínima
- Coste del ciclo de vida mínimo
- Flete requerido mínimo
- Tasa de recuperación de capital propio máxima
- Tasa de rentabilidad interna máxima

En este caso, se utilizará el criterio de coste de construcción mínimo, ya que es el empleado por los astilleros para establecer las características a definir de un buque ya contratado con un valor de oferta mínimo.

Primero debemos calcular el peso en rosca y optimizar resultados

11-CÁLCULO DEL PESO EN ROSCA

El cálculo del peso en rosca lo vamos a dividir en tres partes:

- Acero
- Equipo y habilitación
- Maquinaria

Cálculo del peso de acero

Esta expresión nos permite realizar un cálculo rápido y aproximado del peso de acero del buque.

$$W_{ST} = K \cdot L \cdot B \cdot D \cdot \left(\frac{L}{D}\right)^{1/2} = 29.631,3 t.$$

Peso del equipo y la habilitación

$$W_{OA} = K_e \cdot L_{pp} \cdot B = 2.540,46 t.$$

Donde:

K_e : para buques gaseros:

$$K_e = 0,36 - 0,53 \cdot 10^{-3} \cdot L_{pp} = 0,2161$$

L_{pp} : eslora entre perpendiculares (271,5 m.)

B: manga de trazado (43,3 m.)

Peso de maquinaria

$$\text{Total peso maquinaria} \rightarrow W_Q = W_{PM} + W_{QR} + W_{QE} = 3.090,05 t.$$

Peso de la maquinaria principal (motor y resto de la maquinaria propulsora)

$$W_{PM} = a \cdot \left(\frac{BHP}{rpm}\right)^b + c \cdot BHP^d = 2353 t.$$

Donde:

BHP: potencia necesaria

Para calcularla utilizaremos la fórmula de Watson:

$$BHP = \frac{0,889 \cdot \Delta^{2/3} \cdot \left(40 - \frac{L_{PP}}{61} + 400 \cdot (K - 1)^2 - 12CB\right)}{15.000 - 1,81 \cdot N \cdot \sqrt{L_{PP}}} V^3 = 36.036,3 \text{ HP}$$

$$BKW = 36.036,3 \cdot 0,746 = 26.883,1 \approx 26.884 \text{ kW}$$

Donde:

-N: número de revoluciones del motor, tomaremos como referencia 90 de una estimación media de los buques de la base de datos.

-K: constante de la fórmula de Alexander

$$CB = K - \frac{0,5 \cdot V}{\sqrt{3,28 \cdot L_{PP}}} \rightarrow K = 1,0955$$

Donde:

-CB: coeficiente de bloque (0,7688).

-V: velocidad de servicio (19,5 knots).

-Lpp: eslora entre perpendiculares (271,5 m.).

- Δ : desplazamiento de nuestro buque (al calado de diseño) = 106.536 t.

-rpm: revoluciones por minuto del motor (90 rpm)

-a, b, c y d: constantes $\rightarrow a = 9,38, b = 0,84, c = 0,59$ y $d = 0,70$

Peso de la maquinaria y el equipo restante

$$W_{QR} = 0,03 \cdot V_{MQ} = 623,62 \text{ t.}$$

Donde:

- V_{MQ} : volumen de la cámara de máquinas, que podemos calcular de manera aproximada mediante la siguiente fórmula:

$$V_{MQ} = \frac{L}{5} \cdot B \cdot T \cdot C_B = 20.787,34 \text{ m}^3$$

Donde:

-L: eslora entre perpendiculares (271,5 m.)

-T: calado de diseño (11,50 m.)

-B: manga máxima (43,3 m.).

-D: puntal a la cubierta principal (26 m.).

Peso de línea de ejes fuera de la cámara de máquinas

$$W_{QE} = K_{ne} \cdot l_{eje} (5 + 0,0164 \cdot L_{pp}) = 113,43 \text{ t.}$$

Donde:

- K_{ne} : 2 en buques de dos líneas de ejes.

- l_{eje} : longitud en metros de la línea de ejes fuera de la cámara de máquinas (tomaremos como referencia 6 m.).

-Lpp: eslora entre perpendiculares (271,5 m.).

Por tanto, tendremos que el peso en rosca (LWT) es:

$$LWT = W_{ST} + W_{OA} + W_Q = 35.261,81 \approx 35.262 \text{ t.}$$

Como ya hemos visto, los valores se han redondeado hacia arriba.

Utilizando el valor del desplazamiento calculado anteriormente:

$$DWT = \Delta - LWT = 71.274 \text{ t.}$$

12-COSTES

A la hora de realizar la evaluación económica del buque, nos centraremos en el coste de construcción. Emplearemos como guía las fórmulas y nomenclatura del libro "El Proyecto Básico del Buque Mercante". En muchos de los coeficientes se realizará una aproximación o se tomará un valor medio dentro del determinado rango.

El cálculo del coste de construcción se desglosará en las siguientes partidas:

- Coste del material a granel (CMg)
- Coste de los equipos (Ceq) y su montaje (CmE)
- Coste de la mano de obra (Cmo)
- Costes varios aplicados (Cva)

Coste del material a granel

$$CMg = cmg \cdot W_{ST} = ccs \cdot cas \cdot cem \cdot ps \cdot W_{ST} = 32.307.261,22 \text{ €}$$

Donde:

ccs: coeficiente de coste ponderado de las chapas y perfiles de las distintas calidades de acero del buque (1,07).

Cas: coeficiente de aprovechamiento del acero (1,11).

Cem: coeficiente de incremento por equipo metálico incluido en la estructura tales como tecele, registros, escotillas, etc. (1,08)

ps: precio unitario del acero (850 €/t)

W_{ST}: peso del acero (29.631,3 t)

Coste de los equipos (Ceq) y su montaje (CmE)

$$CEq + CmE = CEc + CEp + CHf + CEr = 18.162.463,42 \text{ €}$$

Donde:

CEc: coste de los equipos de manipulación y contención de la carga. Es una partida de difícil sistematización y se debe estudiar pormenorizadamente para cada tipo de buque.

CEp: coste de los equipos de propulsión y sus auxiliares, montaje incluido

$$CEp = cep \cdot PB = 10.753.600 \text{ €}$$

Donde:

cep: coeficiente de coste unitario (400 €/Kw)

PB: potencia propulsora (26.884 Kw)

CHf: coste, montada, de la habilitación y fonda

$$CHf = chf \cdot nch \cdot NT = 1.270.500 \text{ €}$$

Donde:

chf: coeficiente de coste unitario de la habilitación por tripulante (aprox. 33.000 €/tripulante)

nch: nivel de calidad de la habilitación (1,10)

NT: número de tripulantes (35)

Cer: coste del equipo restante instalado

$$CEr = cer \cdot WEr = 6.138.363,42 \text{ €}$$

Donde:

Ccer: coeficiente de coste unitario por peso

$$cer = pst \cdot cpe = ccs \cdot cas \cdot cem \cdot ps + chm \cdot csh = 2.590,3$$

Donde:

chm: costo horario medio del astillero (30 €/h).

csh: coeficiente de horas por unidad de peso (50 h/t). Está relacionado con la capacidad productiva del astillero.

Wer: peso del equipo restante

$$WEr = K \cdot L^{1,3} \cdot B^{0,8} \cdot D^{0,3} = 2.369,75 \text{ t.}$$

Donde:

K: coeficiente (0,03)

Coste de la mano de obra (Cmo)

$$CMo = CmM + CmE$$

En este apartado incluiremos solamente el coste de montaje de material (CmM), puesto que el coste de montaje de equipos (CmE) ya lo hemos incluido en el apartado de "Coste de equipos y su montaje".

$$CmM = chm \cdot csh \cdot W_{ST} = 44.446.950 \text{ €}$$

Costes varios aplicados (Cva)

Este apartado representa los costes para el astillero de todo aquello que sin intervenir directamente en el proceso de construcción del buque, tiene un coste directo. Estos pueden ser: Sociedades de Clasificación, ensayos en canal, representación...

$$CVa = cva \cdot CC = cva \cdot (CMg + CEq + CmE + CMo) = 6.644.167,23 \text{ €}$$

Donde:

cva: representa el coeficiente de los costes varios del astillero referidos al costo de construcción del buque (0,07).

Por tanto, tendremos que el coste de construcción del buque (CC) es:

$$CC = CMg + CEq + CmE + CMo + CVa \approx 101.560.845 \text{ €}$$

13-ALTERNATIVA MÁS FAVORABLE

Para encontrar la alternativa más favorable vamos a minimizar el coste de construcción utilizando la herramienta "Solver" del programa informático Microsoft Excel. Adjuntamos las hojas de resultados como anexo.

Para ello añadiremos una serie de restricciones a nuestras variables L, B, D y T y a algunas de las relaciones entre ellas.

Restricciones de la base de datos

Utilizando los valores de las dimensiones que aparecen en nuestra vamos de datos vamos a restringir el cálculo.

	L/B	B/D	B/T	L/D	T/D	L/T
MÁXIMO	6,45 16	1,8 023	4,1 704	10,9 147	0,4 512	23,94 96
MÍNIMO	6,05 59	1,6 385	3,7 281	10,2 308	0,4 313	23,13 04
VALOR MEDIO	6,21 21	1,6 915	3,8 353	10,5 055	0,4 411	23,81 79

Restricciones de las dimensiones principales

Vamos a darle un margen de variación de un 5% a nuestras dimensiones originales principales, de manera que obtendremos un valor máximo y otro mínimo para cada una de nuestras dimensiones. Entre estos dos valores estarán los definitivos a calcular.

Restricción de volumen

Tomamos la restricción de volumen de las RPA del buque (145.000 m³). Por tanto, haremos variar el volumen en un 1 %, tomando como valor mínimo el de nuestras RPA.

En la siguiente tabla se muestran los valores originales y los valores finales de nuestro buque.

	CONF. INICIAL	CONF. FINAL	
L	271,5	269,7	m
B	43,3	43,2	m
D	26	26,3	m
T	11,5	11,5	m
Volumen	145.000	145.000	m ³
Δ	106.536	105.379	t.
V	19,5	19,5	kn ot
Fn	0,1943	0,1950	-
Cb	0,7688	0,7673	-
Cm	0,9971	0,9971	-
Cp	0,792	0,7905	-
COSTE	101.560 .845	101.099 .769	€

Como podemos ver, se cumplen nuestras restricciones, incluida la del volumen (145.000 m³) al tiempo que se minimiza el coste de construcción.

Señalar que el cálculo de los nuevos coeficientes se detalla en el siguiente apartado. Como se puede observar y era de prever, apenas varían de una configuración a otra.

Con las nuevas dimensiones tendríamos un ahorro de 461.076 €.

14-NUEVO CÁLCULO DE COEFICIENTES

Por tratarse de un barco de volumen utilizaremos las siguientes expresiones para la determinación de V_h (volumen del casco):

$$V_h = C_{BD} \cdot L \cdot B \cdot D$$

$$\underline{V_h = 262.634,6 \text{ m}^3}$$

$$C_{BD} = C_B + C \cdot \frac{D-T}{T} (1 - C_B)$$

$$\underline{C_{BD} = 0,8571}$$

Donde:

$C = 0,3$, para formas en U

C_B : coeficiente de bloque (0,7673), calculado un par de líneas más abajo.

Número de Froude

$$Fn = \frac{V}{\sqrt{g \cdot L}}$$

$$\underline{Fn = 0,1950}$$

Donde:

V : velocidad de servicio (19,5 knot \approx 10,03 m/s)

g : aceleración de la gravedad (9,81 m/s²)

L_{pp} : eslora entre perpendiculares (269,7 m.)

Coficiente de la maestra

$$C_m = 1 - 2 \cdot Fn^4$$

$$\underline{C_m = 0,9971}$$

Coficiente prismático

$$C_p = 1.2 - 2.1 \cdot Fn$$

$$\underline{C_p = 0,7905}$$

Coficiente de bloque

$$C_B = C_m \cdot C_p$$

$$\underline{C_B = 0,7882}$$

A continuación vamos utilizar otra serie de fórmulas para calcular el coeficiente de bloque

Alexander:

$$C_B = 1.08 - 1.68 \cdot Fn$$

$$\underline{C_B = 0,7524}$$

Van Lameren:

$$C_B = 1.137 - 2.02 \cdot Fn$$

$$\underline{C_B = 0,7431}$$

Ayre:

$$C_B = 1.05 - 1.68 \cdot Fn$$

$$\underline{C_B = 0,7224}$$

Minorsky:

$$C_B = 1.22 - 2.38 \cdot Fn$$

$$\underline{C_B = 0,7559}$$

Katsoulis:

$$C_B = 0.8217 \cdot f \cdot L^{0.42} \cdot B^{-0.3072} \cdot D^{0.1721} \cdot V^{-0.6135}$$

$$\underline{C_B = 0,8002}$$

Donde:

f: es un factor de corrección por tipo de buque. En el caso de un gasero toma el valor de 1,04.

$$C_B = a - b \cdot Fn$$

Del punto 9, ya tenemos los valores de a y b, que son:

$$a = 2,023$$

$$b = 6,224$$

Por tanto, para nuestro caso tendremos un $\underline{C_B = 0,8093}$

Haciendo una media de todos los valores obtenidos para el coeficiente de bloque: $C_B = 0,7673$. Y por tanto, como primera aproximación:

$$\Delta = C_B \cdot \rho \cdot L \cdot B \cdot T = 105.378,4 \approx 105.379 \text{ t.}$$

Donde:

$$C_B = 0,7673$$

ρ : densidad del agua salada (1,025 t/m³)

L → Lpp: eslora entre perpendiculares (269,7 m.)

B: manga de trazado (43,2 m.)

T: calado de diseño (11,5 m.)

15-ESTIMACIÓN DE POTENCIA

Estimación mediante fórmula de Watson

Para calcularla utilizaremos la fórmula de Watson:

$$BHP = \frac{0,889 \cdot \Delta^{2/3} \cdot (40 - \frac{L_{PP}}{61} + 400 \cdot (K - 1)^2 - 12CB)}{15.000 - 1,81 \cdot N \cdot \sqrt{L_{PP}}} V^3 = 35.783,9 \text{ HP}$$

$$BKW = 35.783,9 \cdot 0,746 = 26.694,8 \approx 26.695 \text{ kW}$$

Donde:

-N: número de revoluciones del motor, tomaremos como referencia 90 de una estimación media de los buques de la base de datos.

-K: constante de la fórmula de Alexander

$$CB = K - \frac{0,5 \cdot V}{\sqrt{3,28 \cdot L_{PP}}} \rightarrow K = 1,0951$$

Donde:

-CB: coeficiente de bloque (0,7673).

-V: velocidad de servicio (19,5 knots).

-Lpp: eslora entre perpendiculares (269,7 m.).

-Δ: desplazamiento de nuestro buque (al calado de diseño) = 105.379 t.

Estimación mediante NAVCAD

Eslora en la flotación

No tenemos todavía este dato. Por tanto, tomaremos como aproximación:

$$L_{WL} = 1,04 \cdot L_{pp} = 280,5 \text{ m.}$$

Bulbo de proa

No tenemos todavía estos dato. Por tanto, tomaremos como aproximación los del buque de la base de datos "Express", que tiene unas dimensiones parecidas. (Se adjutan características y plano en los anexos).

Altura (h)

$$h = 4,30 \text{ m.}$$

Protuberancia (x)

$$x = 6,55 \text{ m.}$$

Coeficiente de área de la flotación

$$C_F = \frac{1 + 2 \cdot C_B}{3} = 0,8448$$

Área del plano de la flotación

$$Waterplane Area = L \cdot B \cdot C_F = 9.842,799 \text{ m}^2$$

Coeficiente de área de la maestra

$$C_m = 0,9971$$

Área de la sección máxima (maestra)

$$Max. Section Area = B \cdot T \cdot C_m = 495,359 \text{ m}^2$$

Superficie mojada

$$S = L_{WL}(2T + B)C_m^{0,5} \left(0,453 + 0,4425C_B - 0,2862C_m - 0,003467 \cdot \frac{B}{T} + 0,3696C_F \right) + 2,38 \frac{ABT}{C_B} = 14.983,25 \text{ m}^2$$

Donde:

ABT: área transversal del bulbo en la perpendicular de proa. Lo calculamos a partir de una tabla del libro “El Proyecto Básico del Buque Mercante”.

Interpolando en esta tabla con los valores de L/B = 6,2430 y C_b = 0,7673, tenemos que:

$$ABT = 10,1 \text{ m}^2$$

Otros datos que introducimos en NAVCAD son:

Densidad del agua = 1,025 t/m³

Viscosidad cinemática = 1,18830 · 10⁻⁶ m²/s

Margen de diseño: 15 %

Con todos estos datos obtenemos los siguientes resultados:

SPEED [kt]	RESISTANCE AND EFFECTIVE POWER								
	RBARE [kN]	RAPP [kN]	RWIND [kN]	RSEAS [kN]	RCHAN [kN]	RMARGIN [kN]	RTOTAL [kN]	PEBARE [kW]	PETOTAL [kW]
17,50	1658,96	82,95	0,00	0,00	0,00	248,84	1990,75	14935,3	17922,3
18,00	1760,55	88,03	0,00	0,00	0,00	264,08	2112,66	16302,7	19563,3
18,50	1867,55	93,38	0,00	0,00	0,00	280,13	2241,06	17773,9	21328,7
19,00	1980,36	99,02	0,00	0,00	0,00	297,05	2376,43	19356,9	23228,3
+ 19,50 +	2099,41	104,97	0,00	0,00	0,00	314,91	2519,30	21060,6	25272,8
20,00	2225,23	111,26	0,00	0,00	0,00	333,78	2670,27	22895,1	27474,1
20,00	2225,23	111,26	0,00	0,00	0,00	333,78	2670,27	22895,1	27474,1
20,50	2358,17	117,91	0,00	0,00	0,00	353,73	2829,81	24869,5	29843,4
21,00	2498,40	124,92	0,00	0,00	0,00	374,76	2998,08	26991,1	32389,3
21,50	2646,08	132,30	0,00	0,00	0,00	396,91	3175,29	29267,1	35120,5

Vemos que para nuestra velocidad de servicio (19,5 knot) necesitamos una potencia de 25.272,8 kW. Pero debemos destacar que esta potencia corresponde a la EHP (potencia efectiva o de arrastre). Habría que tener en cuenta el rendimiento del conjunto de la propulsión (algo que haremos en el cuaderno 6). Teniendo en cuenta esto, vemos que difiere un tanto de la calculada por la fórmula de Watson, pero para una primera aproximación es válida.

Para los cálculos en que sea necesaria la potencia en el presente cuaderno, utilizaremos la calculada por la fórmula de Watson, puesto que ésta sí se refiere a la BHP (potencia al freno).

16-NUEVO CÁLCULO DEL PESO EN ROSCA, PESO MUERTO, DESPLAZAMIENTO Y CONSUMOS

Con los valores optimizados de nuestras dimensiones, vamos a calcular de nuevo los pesos.

PESO EN ROSCA

El cálculo del peso en rosca lo vamos a dividir en tres partes:

- Acero
- Equipo y habilitación
- Maquinaria

Cálculo del peso de acero

Esta expresión nos permite realizar un cálculo rápido y aproximado del peso de acero del buque.

$$W_{ST} = K \cdot L \cdot B \cdot D \cdot \left(\frac{L}{D}\right)^{1/2} = 29.437,72 \text{ t.}$$

Donde:

$$K = 0,03$$

Peso del equipo y la habilitación

$$W_{OA} = K_e \cdot L_{pp} \cdot B = 2.528,28 \text{ t.}$$

Donde:

K_e : para buques gaseros:

$$K_e = 0,36 - 0,53 \cdot 10^{-3} \cdot L_{pp} = 0,21,70$$

L_{pp} : eslora entre perpendiculares (269,7 m.)

B : manga de trazado (43,2 m.)

Peso de maquinaria

$$\text{Total peso maquinaria} \rightarrow W_Q = W_{PM} + W_{QR} + W_{QE} = 3.013,49 \text{ t.}$$

Peso de la maquinaria principal (motor y resto de la maquinaria propulsora)

$$W_{PM} = a \cdot \left(\frac{BHP}{rpm}\right)^b + c \cdot BHP^d = 2.340,1 \text{ t.}$$

Donde:

-BHP: potencia necesaria (35.784 HP)

-rpm: revoluciones por minuto del motor (90 rpm)

-a, b, c y d: constantes $\rightarrow a = 9,38$, $b = 0,84$, $c = 0,59$ y $d = 0,70$

Peso de la maquinaria y el equipo restante

$$W_{QR} = 0,03 \cdot V_{MQ} = 616,85 \text{ t.}$$

Donde:

- V_{MQ} : volumen de la cámara de máquinas, que podemos calcular de manera aproximada mediante la siguiente fórmula:

$$V_{MQ} = \frac{L}{5} \cdot B \cdot T \cdot C_B = 20.561,64 \text{ m}^3$$

Donde:

-L: eslora entre perpendiculares (269,7 m.)

-T: calado de diseño (11,50 m.)

-B: manga máxima (43,2 m.).

Peso de línea de ejes fuera de la cámara de máquinas

$$W_{QE} = K_{ne} \cdot l_{eje}(5 + 0,0164 \cdot L_{PP}) = 56,54 \text{ t.}$$

Donde:

- K_{ne} : 2 en buques de dos líneas de ejes.

- l_{eje} : longitud en metros de la línea de ejes fuera de la cámara de máquinas (tomaremos como referencia 6 m.).

- L_{pp} : eslora entre perpendiculares (269,7 m.).

Por tanto, tendremos que el peso en rosca (LWT) es:

$$LWT = W_{ST} + W_{OA} + W_Q = 34.979,49 \approx 34.980 \text{ t.}$$

Como ya hemos visto, todos los valores se han redondeado hacia arriba.

DESPLAZAMIENTO

Nuestro nuevo desplazamiento será:

$$\Delta = 1,025 \cdot L \cdot B \cdot T \cdot C_B \approx 105.379 \text{ t.}$$

PESO MUERTO

Utilizando el valor del desplazamiento calculado anteriormente:

$$DWT = \Delta - LWT = 70.399 \text{ t.}$$

El peso muerto es la suma de la carga útil y los consumos

Carga útil

$$145.000 \text{ m}^3 \cdot 0,45 \frac{\text{t}}{\text{m}^3} = 65.250 \text{ t.}$$

Donde:

$$\rho_{LNG} = 0,45 \text{ t/m}^3$$

Consumos

En este cuaderno realizaremos una primera aproximación a los consumos. En el cuaderno 4 se calcularán más detalladamente.

Peso del combustible

$$P_{COMB} = \text{Autonomía}(h) \cdot BHP \cdot C_e \cdot 10^{-6} = 3.741,22 \text{ t.}$$

Donde:

C_e : consumo específico del motor principal. Según el libro "Proyecto de Buques y Artefactos", el consumo para motores electrógenos oscila entre 160-180 gr/BHP por hora. Por tanto, tomamos un consumo aproximado de 170 gr/BHP

BHP: potencia propulsora (35.784 Kw)

Autonomía: 12.000 millas a 19,5 knot. Señalar que un nudo (knot) es igual a una milla marina (mn) por hora.

$$t_{navegación} = \frac{Autonomía}{Velocidad} = 615,38 \approx 25 \text{ días}$$

Peso del agua dulce

200 litros por persona y día. 25 días de autonomía 35 personas a bordo.

$$Agua \text{ dulce} = 200 \cdot 25 \cdot 35 \cdot 10^{-3} = 175 \text{ t.}$$

Peso del aceite

Se calcula en función del porcentaje de combustible. Se estima entre un 3-4 % del peso del combustible

$$P_{ACEITE} = 0,035 \cdot P_{COMB} = 130,94 \text{ t.}$$

Efectos y respestos: 100 t.

Tripulación y varios: 20 t.

En total tenemos: $P_{MUERTO} \approx 69.417,16 \approx 69.418 \text{ t.}$

Margen de peso muerto: $70.399 - 69.296 = 981 \text{ t.}$

17-CÁLCULO DEL FRANCOBORDO

En esta primera etapa vamos a realizar un cálculo sencillo del francobordo por medio del programa Arqnaval, en el que, introduciendo solamente los datos de eslora, manga, puntal y coeficiente de bloque, nos arroja un primer resultado de nuestro francobordo y una altura mínima de proa.

Debemos señalar en el cálculo el tipo de buque que estamos proyectando, como no hay la opción de LNG, escogemos un LPG.





De acuerdo con el “Convenio internacional sobre líneas de carga de 1966”, nuestro buque es tipo A. Y debemos tener:

Francobordo (FB)

$$FB = 6,366 \text{ m.}$$

Con lo que el buque tendría un calado en esta condición máxima de 19,961 m.

Altura mínima de proa (F_b)

$$F_b = 6,536 \text{ m.}$$

En el cuaderno 9 calcularemos nuestro francobordo real de una forma mucho más detallada y precisa, esto es sólo una aproximación.

18-ESPECIFICACIÓN PRELIMINAR

En este apartado vamos a detallar la operación básica del buque así como algunos de los distintos equipos necesarios para la misma.

Partimos del buque en puerto, con los tanques en condiciones ambiente: presión, temperatura y composición. La carga del buque la constituye gas licuado, con una composición del 98% en metano, a presión ambiente y temperatura de -163°C, que será aproximadamente la de cambio de fase líquido-gas de la carga. Como no nos interesa bajar la temperatura al no existir variaciones apreciables en la densidad de la carga, y sí encarecer el coste de enfriamiento y aislamiento.

El tipo de carga nos condiciona el buque en los siguientes aspectos:

- Los relativos a la seguridad en las maniobras de carga y descarga, debiendo evitarse la presencia de una atmósfera peligrosa en los tanques al introducir el gas.
- La temperatura de carga puede dañar el tanque por choque térmico, luego debemos acondicionarlo previamente.
- El tratamiento del “39oíl-off”.

Maniobra de carga de los tanques

Preparación de la atmósfera dentro de los tanques

Esta operación se lleva a cabo después de la nueva construcción o de un viaje en seco, y antes de una operación de carga.

-Purga de aire: se hará circular por el tanque gas inerte (CO₂), para hacer una "limpieza" y eliminar así el oxígeno y la humedad presentes en el aire. Para ello se necesitará un generador de gas inerte, que podemos materializar mediante una extracción de los gases de escape de la caldera, motor principal o auxiliares o de un generador de gas inerte que funcione como generador de aire seco. El objetivo de esta operación es bajar el punto de rocío a -20°C antes de la inertización.

-Inertización de los tanques: después de purgar el tanque de aire, se inertizará el mismo por medio del generador de gas inerte o usando el vaporizador principal produciendo GN₂ a partir de LN₂ suministrado por la terminal. El gas inerte al ser más pesado que el aire se introduce por el fondo del tanque, mientras que el GN₂ al ser más ligero se introduce por arriba. En ambos casos la operación se seguirá hasta que se alcance un contenido de oxígeno menor del 2 % y un punto de rocío más bajo de -40°C.

-Inertización de tuberías y maquinaria: esta operación se realiza durante la inertización de los tanques. Se debe comprobar que todas las líneas que no se usen para la inertización de los tanques han sido purgadas.

Necesitaremos para este proceso de los compresores y líneas de alimentación para introducir los gases en los tanques y para su posterior evacuación, así como sendos generadores de gas inerte CO₂ y N₂.

Acondicionamiento térmico de los tanques de carga

Debido a que la carga la vamos a recibir y a transportar a una temperatura aproximada de unos -163 °C, no es posible descargar directamente sin previamente enfriar los tanques a una temperatura cercana a ese valor, pues el choque térmico que provocaríamos dañaría los mismos permanentemente. Así mismo, las tuberías procedentes de la terminal y las del buque, deberán también estar a temperatura adecuada.

Esta problemática será analizada en el cuaderno 12.

Tratamiento del gas evaporado o "Boil off" durante la navegación

Durante la navegación normal del buque, un tanto por ciento de la carga se va evaporando, debido al calor que reciben los tanques del exterior. Podemos acometer este problema de tres maneras:

- Descargándolo a la atmósfera
- Reenviándolo a los tanques de carga, previamente re-criogenizado.
- Emplearlo para la combustión en los generadores

Nosotros lo utilizaremos para estos dos últimos procedimientos.

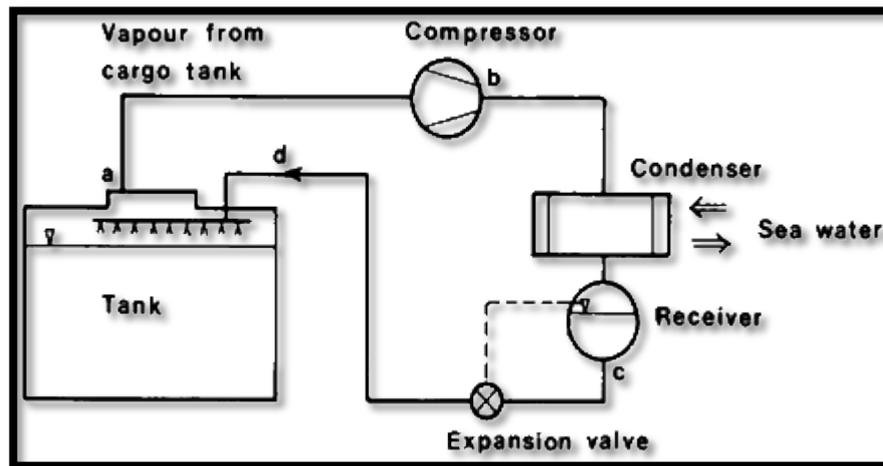
Boil off

El aislamiento de los tanques será el necesario para mantener en el viaje normal una tasa de evaporación no superior al 0.15 % del peso total.

Relicuefacción

Si queremos reenviar el gas evaporado de los tanques nuevamente a ellos, deberemos contar en el buque con una planta de relicuefacción, que sea capaz de licuar todo el gas que se evapora.

En la siguiente imagen podemos ver un esquema de lo que sería una planta de relicuefacción.



Construcción de los tanques

Los tanques y equipos de carga se diseñarán para almacenar gas licuado en cuatro tanques a presión atmosférica a una temperatura de $-163\text{ }^{\circ}\text{C}$.

Los tanques serán de tipo membrana TECNIGAZ GAZ-TRANSPORT. Cada uno de los tanques consta de una barrera primaria y otra secundaria, soportadas por los aislamientos primario y secundario.

- Aislamiento secundario: caja de conglomerado de 0.3 m de espesor, relleno de perlita y soportado por el casco.

- Barrera secundaria: lámina de acero al níquel al 36%, que unida al aislamiento secundario forma una barrera para evitar el escape del gas.

- Aislamiento primario: de igual construcción que el secundario, de 0.23 m de espesor y unido rígidamente al casco.

- Barrera primaria: de la misma composición que la barrera secundaria. Contiene el gas.

Conexiones de los tanques de carga

Cada uno de los tanques de carga tiene una entrada de gas situada cerca del punto más alto del tanque.

La entrada de carga principal y el acceso al tanque se encuentra en la parte más a popa del tanque, que llamaremos entrada de gas líquido.

Los tanques tendrán las siguientes conexiones:

PARTE DE POPA (LIQUIDO)

- Entrada de la bomba principal de carga, con válvula de asiento, compartida con la bomba de emergencia.
- Dos tomas para las bombas de descarga.
- Una línea de descarga del gas de rociado.
- Sensores térmicos, de nivel.
- Línea principal.
- Medidores de nivel
- Conexiones eléctricas y de instrumentación.

PARTE SUPERIOR (GAS)

- Dos sistemas de rociado
- Conexiones de las válvulas de seguridad

Equipos para el manejo de la carga

- Bombas de carga
- Bombas de emergencia
- Compresores principales
- Compresores auxiliares
- Generador de nitrógeno
- Generador de gas inerte

Tipo de propulsión

El tipo de propulsión de nuestro buque, definida en las RPA será diesel-eléctrica. En el cuaderno 6 especificaremos los elementos que la compondrán.

La capacidad de un motor eléctrico para proporcionar un par elevado a baja velocidad es un argumento importante a favor de la propulsión eléctrica.

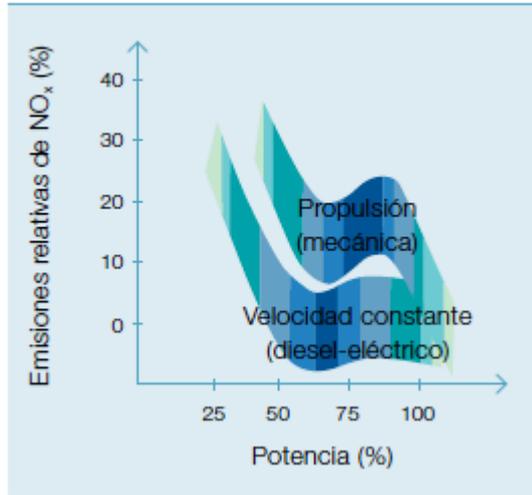
La introducción de la propulsión eléctrica requiere la sustitución del eje entre el motor principal y la hélice por un sistema compuesto por generadores, cuadros de distribución, transformadores, accionamientos y motores.

Los motores diesel no tienen el mismo nivel de contaminación en todo su rango de trabajo. En el régimen óptimo de operación, el rendimiento del combustible es considerablemente mayor y la contaminación es menor que operando a baja velocidad.

En el siguiente gráfico podemos ver cómo los niveles de contaminación para distintos porcentajes de potencia. Vemos que a potencias bajas, la contaminación es

similar que la de los motores mecánicos, pero a mayores potencias es sustancialmente menor.

8 Se emite menos NO_x si la carga en el motor es alta (Fuente: Wärtsilä Diesel).



19-BIBLIOGRAFÍA

-“El Proyecto Básico del Buque Mercante”; Ricardo Alvariño, Juan José Azpíroz y Manuel Meizoso.

-“Proyectos de Buques y Artefactos”, Fernando Junco Ocampo.

-Apuntes asignatura “Métodos Computacionales Aplicados al Proyecto del Buque”, EPS Ferrol.

-Diverso material web.

ANEXO I

Informe herramienta Solver

Microsoft Excel 12.0 Informe de respuestas

**Hoja de cálculo: [Alternativas
final.xlsx]Alternativas**

Celda objetivo (Mínimo)

C elda	Nombre	Valor original	Valor final
\$ K\$4	Coste total	101560845	101099768 ,4

Celdas cambiantes

C elda	Nombre	Valor original	Valor final
\$ C\$3	L	271,5	269,73594 58
\$ C\$4	B	43,3	43,199197 25
\$ C\$5	D	26	26,365088 34
\$ C\$6	T	11,5	11,5

Restricciones

C elda	Nombre	Valor de la celda	Fórmula	Estad o	Diverge ncia
\$ E\$14	L/B buque	Valores de nuestro 6,24400366 2	\$E\$14<=\$ C\$14	Opcio nal	0,20759 6338
\$ E\$14	L/B buque	Valores de nuestro 6,24400366 2	\$E\$14>=\$ D\$14	Opcio nal	0,18810 3662
\$ E\$15	B/D buque	Valores de nuestro 1,6385	\$E\$15<=\$ C\$15	Opcio nal	0,1638
\$ E\$15	B/D buque	Valores de nuestro 1,6385	\$E\$15>=\$ D\$15	Obliga torio	0
\$ E\$16	B/T buque	Valores de nuestro 3,75645193 5	\$E\$16<=\$ C\$16	Opcio nal	0,41394 8065
\$ E\$16	B/T buque	Valores de nuestro 3,75645193 5	\$E\$16>=\$ D\$16	Opcio nal	0,02835 1935
\$ E\$17	L/D buque	Valores de nuestro 10,2308	\$E\$17<=\$ C\$17	Opcio nal	0,6839

\$ E\$17	L/D buque	Valores de nuestro	10,2308	\$E\$17>=\$ D\$17	Obliga	0
\$ E\$18	T/D buque	Valores de nuestro	0,43618287	\$E\$18<=\$ C\$18	Opcio	0,01501
\$ E\$18	T/D buque	Valores de nuestro	0,43618287	\$E\$18>=\$ D\$18	Opcio	0,00488
\$ E\$19	VOL buque	Valores de nuestro	145000	\$E\$19<=\$ C\$19	Opcio	1450
\$ E\$19	VOL buque	Valores de nuestro	145000	\$E\$19>=\$ D\$19	Obliga	0
\$ C\$3	L		269,735945	\$C\$3<=\$ D \$3	Opcio	15,3390
\$ C\$3	L		269,735945	\$C\$3>=\$ E \$3	Opcio	11,8109
\$ C\$4	B		43,1991972	\$C\$4<=\$ D \$4	Opcio	4,43080
\$ C\$4	B		43,1991972	\$C\$4>=\$ E \$4	Opcio	4,22919
\$ C\$5	D		26,3650883	\$C\$5<=\$ D \$5	Opcio	2,23491
\$ C\$5	D		26,3650883	\$C\$5>=\$ E \$5	Opcio	2,96508
\$ C\$6	T		11,5	\$C\$6<=\$ D \$6	Opcio	1,15
\$ C\$6	T		11,5	\$C\$6>=\$ E \$6	Opcio	1,15

Microsoft Excel 12.0 Informe de sensibilidad

Hoja de cálculo: [Alternativas final.xlsx]Alternativas

Celdas cambiantes

C	Nombre	Valor	Gradiente
celda		Igual	reducido
\$ C\$3	L	269,735 9458	0
\$	B	43,1991	0

C\$4		9725	
\$		26,3650	
C\$5	D	8834	0
\$			
C\$6	T	11,5	0

Restricciones

C	Nombre	Valor	Multiplicador de Lagrange
elda		Igual	
\$ E\$14	L/B Valores de nuestro buque	6,24400 3662	0
\$ E\$14	L/B Valores de nuestro buque	6,24400 3662	0
\$ E\$15	B/D Valores de nuestro buque	1,6385	0
\$ E\$15	B/D Valores de nuestro buque	1,6385	3,496203 041
\$ E\$16	B/T Valores de nuestro buque	3,75645 1935	0
\$ E\$16	B/T Valores de nuestro buque	3,75645 1935	0
\$ E\$17	L/D Valores de nuestro buque	10,2308	0
\$ E\$17	L/D Valores de nuestro buque	10,2308	4312178, 102
\$ E\$18	T/D Valores de nuestro buque	0,43618 2874	0
\$ E\$18	T/D Valores de nuestro buque	0,43618 2874	0
\$ E\$19	VOL Valores de nuestro buque	145000	0
\$ E\$19	VOL Valores de nuestro buque	145000	367,9071 414

Microsoft Excel 12.0 Informe de límites

Hoja de cálculo: [Alternativas final.xlsx]Informe de límites 1

Celda objetivo		
Celda	Nombre	Igual
\$		1010997
K\$4	Coste total	68,4

Celdas cambiantes			Límite inferior	Celda objetivo	Límite superior	Celda objetivo
Celda	Nombre	Igual				
\$		269,735	269,735	1010997	271,389	1019041
C\$3	L	9458	9458	68,4	1498	39,6
\$		43,1991	43,1991	1010997	43,1991	1010997
C\$4	B	9725	9725	68,4	9725	68,4
\$	D	26,3650	26,3650	1010997	26,3650	1010997

CUADERNO 1
ISMAEL GRANDAL MOURIZ

C\$5		8834	8834	68,4	8834	68,4
\$			11,3712	1010997	11,5874	1010997
C\$6	T	11,5	626	68,4	5777	68,4

ANEXO II

Buques de la base de datos



ABDELKADER: Tri-fuel DE LNG carrier

Shipbuilder: **Hyundai Heavy Industries Co., Ltd**
 Vessel's name: **Abdelkader**
 Hull No: **1876**
 Owner/operator: **Mitsui OSK Lines (MOL)**
 Country: **Japan**
 Designer: **Hyundai Heavy Industries Co., Ltd**
 Country: **Korea**
 Model test establishment used: **Hyundai Maritime Research Institute**
 Flag: **Bahamas**
 IMO number: **9360922**
 Total number of sister ships already completed (excluding ship presented): **1**
 Total number of sister ships still on order: **0**

HYUNDAI Heavy Industries Co., Ltd (HHI) delivered the vessel *Abdelkader* to Mitsui OSK Lines (MOL) on 27 February. The vessel is a 177,000m³ tri-fuel diesel electric liquefied natural gas (LNG) carrier, which is capable of serving the majority of the Atlantic terminals.

Abdelkader is equipped with four membrane cargo tanks and is designed and constructed as type 2C ship specified in IGC code, suitable for carrying LNG of which vapour pressures are within the range from atmospheric pressure to 0.25bar g.

The vessel features a continuous deck with trunk/without forecabin and has a bulbous bow, lowered mooring deck, transom stern, open water type stern frame, single propeller driven by two electric motors.

Tank insulation is of GTT Mark III system, which has a 270mm thickness to satisfy the low boil off rate of 0.15% by volume of the total cargo per day. A shore manifold is provided on each of the upper decks between No.2 liquid dome and No.3 vapour dome. A compressor room is arranged in the area in way of No.4 tank.

Cargo discharging is done by eight pumps, two located in each of the tanks that each have a capacity of 1750m³/hr. The supplementary gas during discharging comes from shore or is produced by an onboard LNG vapouriser to maintain cargo tank pressure. An emergency cargo pump is used when a cargo pump in a tank fails.

One LD compressor and one spray pump is used when the fuel pump is running to supply fuel gas to the engine room under normal sea going conditions. *Abdelkader* has four sets of main tri-fuelled engines, two have 50% reversible synchronous motors (each with a power converter and associated transformers, control and excitation system), including one reduction gear (twin input/single output) with one propulsion shaft propeller. The vessel has a redundancy, so that failure of any motor drive auxiliary system shall not result in the loss of propulsion power.

The propulsion system onboard *Abdelkader* is a tri-fuelled diesel electric, capable of burning fuel gas, such as natural boil off gas forced boil off gas (FBOG) and also marine diesel oil (MDO) and heavy fuel oil (HFO). The power generating plant utilises all available natural boil off gas (NBOG) and makes up required power by burning additional MDO, HFO or FBOG. The main diesel engines are also fitted with exhaust gas economisers as a waste heat recovery system.

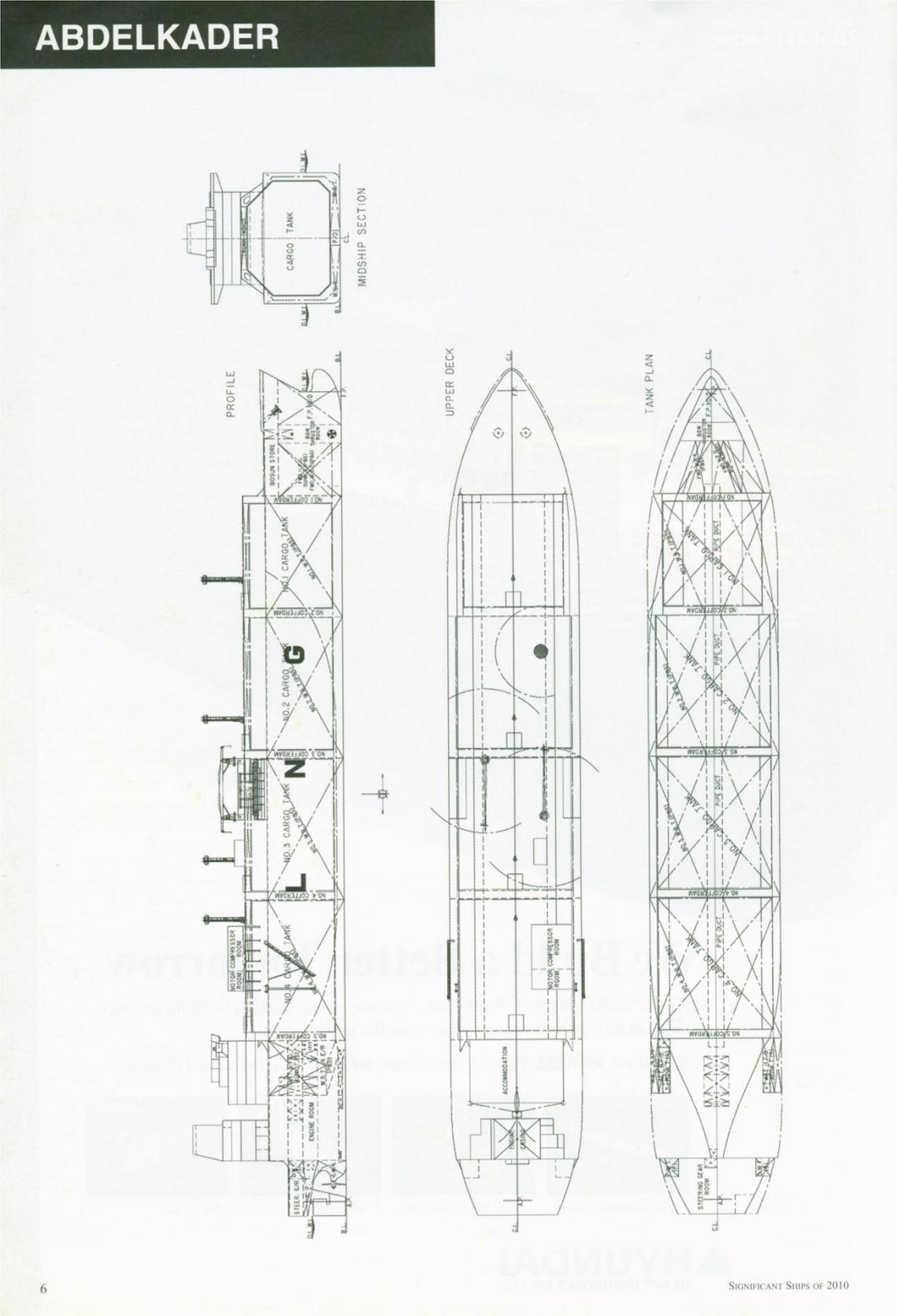
A gas combustion unit is fitted for periods when the NBOG cannot be burned in the tri-fuel diesel engines or when NBOG consumption is low and the cargo tank pressure rises. The tri-fuel diesel engines are fully compliant with MARPOL Annex VI regulation 13 and the NOx technical code.

The engine control room and cargo control room contain all facilities to allow for centralised operations of plant and equipment and also allow for unattended operation of the machinery plant under all operational modes. *Abdelkader's* cargo control room is located in the accommodation deck, where the centralised control of loading, discharging, ballasting and de-ballasting and constant monitoring of the cargo takes place.

TECHNICAL PARTICULARS

Length oa: 298m
 Length bp: 285m
 Breadth moulded: 46m
 Depth moulded: 26.8m
 To main deck: 26.8m
 To upper deck: 26.8m
 To other decks: 34.6m
 Width of double skin
 Side: 2.65m
 Bottom: 3.3m
 Draught
 Scantling: 13.0m
 Design: 11.9m
 Gross: 114,200gt
 Deadweight
 Design: 87,100dwt
 Scantling: 99,700dwt
 Speed, service: 19.6knots
 Cargo capacity
 Liquid volume: 177,400m³
 Bunkers
 Heavy oil: 6800m³
 Diesel oil: 480m³
 Water ballast: 65,000m³
 Daily fuel consumption (based on HFO)
 Main generator engine: 161tonnes/day
 Classification society and notations: Bureau Veritas, BV 1 +HULL, +MACH, Unrestricted navigation, Liquefied gas carrier, +AUTUMS, +VERISTAR-HULL, SYS-NEQ-1, In water survey, MON-SHAFT
 % high tensile steel used in construction: approx. 5%
 Main engine
 Design: Tri-fuel diesel electric
 Model: 2 x 12V50DF 2 x 9L50DF
 Manufacturer: Wartsila
 Number: 4
 Type of fuel used: Fuel gas, HFO or MDO
 Output of each engine: 2 x 11,400kW
 Total 39,900kW
 Gearbox
 Make: Renk
 Model: NDSH-4000
 Number: 1
 Output speed: 90.6rpm
 Propellers
 Material: Ni-Al-Bronze
 Designer/manufacturer: Hyundai
 Number: 1
 Fixed/controllable pitch: Fixed
 Diameter: 8.6m
 Speed: 90.6rpm
 Diesel-driven alternators
 Number: 4
 Engine make/type: Wartsila
 Type of fuel: Fuel gas, HFO or MDO
 Output/speed of each set: Total 39,900kW
 Alternator make/type: Convertteam/ synchronous AC generator

Output/speed of each set: 2 x 11,000kW/514rpm
 2 x 8250kW/514rpm
 Boilers
 Number: 2 x auxiliary boiler 2 x exhaust gas economiser
 Type: vertical, cylindrical, automatic controlled marine boiler (aux. boiler)
 Vertical, forced circulating, smoke tube (exhaust gas economiser)
 Make: Kangrim
 Output, each boiler: 7500kg/h x 10kg/cm²g saturated steam Exhaust gas 1800kg/h x 10kg/cm²g saturated steam
 Other cranes
 Number: 2 x manifold service
 2 x provision handling 1 x cargo machinery room service
 Make: Oriental Precision Co., Ltd
 Type: Electro-hydraulic driven
 Performance: 5tonnes SWL for manifold and provision handling 6tonnes SWL for cargo machinery room
 Mooring equipment
 Number: 11
 Make: Pusnes
 Type: Electro-hydraulic driven
 Special lifesaving equipment
 Number and capacity: 2
 Make: Norsafe
 Type: Davit launching type
 Cargo tanks
 Number: 4
 Grades of cargo carried: 1
 Stainless steel-structure/piping: SUS 304/SUS 304L
 Cargo pumps
 Number: 8
 Type: Vertical, centrifugal submerged
 Make: Ebara
 Capacity, each: 1750m³ x 175mlc
 Cargo control system
 Make: Convertteam
 Type: AVC
 Bow thruster
 Make: Kawasaki
 Number: 1
 Output, each: 2200kW
 Bridge control system
 Make: Convertteam
 Type: Electric propulsion system
 One-man operation: Yes
 Fire detection system
 Make: Consilium
 Type: Intelligent addressable type
 Fire extinguishing systems
 Engine room: NK/High pressure CO₂
 Cabins: Sea water + fresh water
 Public spaces: Sea water + fresh water
 Radars
 Number: 3
 Make: JRC
 Models: LMA-9932-SA JMA-9922-6xA NKE-1087-6
 Integrated bridge system
 Make: JRC
 Model: JAN-901M, JAN-701-COIN
 Waste disposal plant
 Incinerator: Kangrim KFB-73
 Sewage plant: Jongjap BIO AEROB-18
 Contract date: 06 May 2006
 Launch/float-out date: 10 October 2008
 Delivery date: 27 February 2010





BERGE EVERETT: Daewoo LNG tanker

Shipbuilder: Daewoo Shipbuilding & Marine Engineering Co Ltd (DSME), Korea
 Vessel's name: *Berge Everett*
 Hull number: 2212
 Owner/operator: Bergesen dy, ASA, Norway
 Designer: Daewoo Shipbuilding & Marine Engineering Co Ltd, Korea
 Flag: Norway
 Total number of sister ships already completed: 1
 Total number of sister ships still on order: 1

THE leading positions held in the LNG market by Norwegian owner Bergesen, and shipbuilder Daewoo, is demonstrated by their combined involvement in the construction of *Berge Everett*, another example of the Korean company's circa 140,000m³ capacity, specialist Type 2G gas carrier design, introduced for worldwide trading in a rapidly expanding fuel distribution network. A number of factors required consideration in the development of this class of vessel, many of which relate to parameters existing at loading and discharging terminals, where positions of mooring equipment, fenders, gangway and manifolds are of particular importance.

In addition, in order to ensure an even keel ballast arrival condition with peak tanks empty, and allowing consumables at 50% maximum capacity and three days reserve, the disposition and quantity of water ballast carried has necessitated careful study. The layout is also arranged to enable the vessel to discharge at the Everett (Boston, USA) terminal where an air draught restriction of 41.2m from the ballast waterline is enforced.

Within a double-hull structure there are four cargo tanks separated by cofferdams, and which extend above the upper deck to form a trunk. These are constructed to the Gaz Transport NO96 E-2 membrane system which uses Invar stainless steel sheet with a nickel content of 36%, for primary and secondary barriers, with perlite granules in plywood boxes inserted between them, and between the secondary barrier and the shell. This system, together with hull scantlings and cargo pumps, is suitable for the carriage of cargo of maximum specific gravity 0.50 at -163°C, and maximum boil-off rate 0.15% cargo volume. Underdeck passageways in the trunk deck space provide fore and aft access, and a duct keel in the double bottom carries pipes and cables.

Cargo handling is by means of eight Ebara, aluminium alloy, submerged, centrifugal electric pumps, each with a duty of 1700m³/h and together capable of discharging a full cargo in 12 hours. Other equipment forming part of the cargo system includes high- and

low-duty compressors, main and forcing vaporisers, and boil-off/warm-up heaters. Heavy-fuel tanks are contained within the double hull and have a capacity for 13,000 nautical miles steaming at 90% MCR, allowing five days margin without the use of boil-off gas.

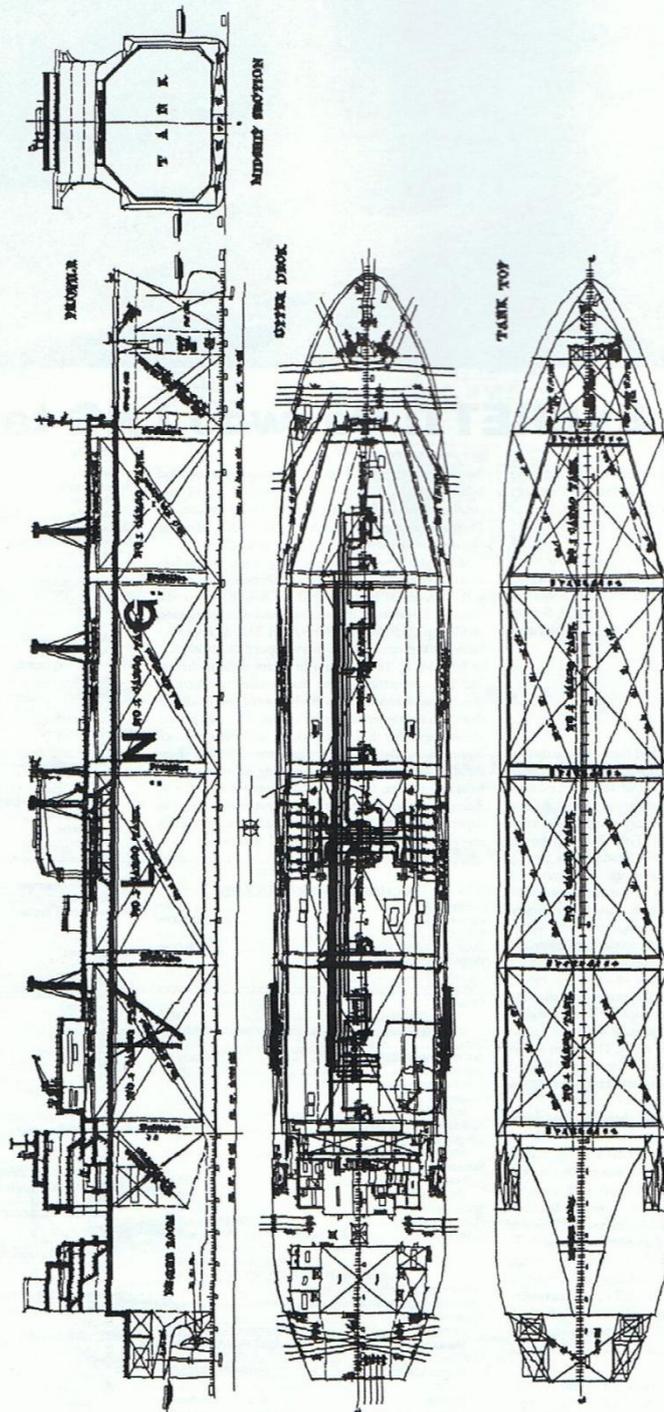
Although Daewoo is looking at the use of alternatives to the 'conventional' steam turbine propulsion system, it is this which has been adopted for *Berge Everett*, in the form of a Kawasaki cross-compound unit developing 36,690shp (26,985kW) at 88rev/min. This drives a five-bladed, FP propeller for a service speed of 19.50knots at 90% MCR. Two Mitsubishi steam-turbine-driven, 3450kW alternators are the main source of electrical power, supplemented by a Rolls-Royce/Bergen-driven diesel-alternator set of similar output. The two boilers are arranged for dual-fuel burning, and each produce 56tonnes/h. Brunvoll supplied the 1600kW bow thruster which provides manoeuvring aid to the semi-balanced rudder, fitted in an open-water sternframe. Accommodation is arranged for 43 persons in the main superstructure aft, with the living quarters completely separate from the engine and funnel casings.

TECHNICAL PARTICULARS

Length, oa 277.00m
 Length, bp 266.00m
 Breadth, moulded 43.40m
 Depth, moulded to upper deck 26.00m
 Width of double skin
 side 2.11m
 bottom 3.20m
 Draught
 design 11.40m
 scantling 12.10m
 Gross 93,844gt
 Displacement 107,000tonnes
 Lightweight 29,600tonnes
 Deadweight
 design 70,300dwt
 scantling 77,400dwt
 Speed, service at 90% MCR 19.50knots
 Cargo capacity
 liquid volume 138,000m³
 Bunkers
 heavy oil 6000m³
 diesel oil 500m³
 Water ballast 52,400m³
 Fuel consumption 168,800tonnes/day
 Classification Det Norske Veritas 1A1, Tanker for Liquefied Gas, Ship type 2G (-163°C, 500kg/m³, 0.25bar), NAUTICUS
 Newbuilding, PLUS-1, EO, W1-OC, LCS (S10)
 Percentage of high-tensile steel used in construction Nil
 Steam turbines
 Design Cross-compound impulse
 Manufacturer Kawasaki Heavy Industries
 Number 1
 Output/speed 26,985kW/88rev/min
 Propeller
 Material Nickel-aluminium-bronze
 Designer/manufacturer Hyundai Heavy Industries
 Number 1
 Pitch Fixed
 Diameter 8500mm

Speed 88rev/min
 Steam-turbine-driven alternators
 Number 2
 Make/type Mitsubishi Heavy Industries/multi-stage
 Output/speed 2 x 3450kW/1800rev/min
 Diesel-driven alternators
 Number 1
 Make/type Rolls-Royce Bergen-
 Output/speed 3450kW/720rev/min
 Boilers
 Number 2
 Type Vertical, 2-drum, water tube
 Make Mitsubishi Heavy Industries
 Output 2 x 56tonnes/h
 Hose-handling cranes
 Number 2
 Make Shinyong-TTS
 Type Electro-hydraulic
 Performance 2 x 12tonnes swl
 Mooring equipment
 Make Rolls-Royce
 Type Electro-hydraulic
 Cargo tanks
 Number 4
 Grades of cargo carried LNG
 Stainless steel Structure and piping
 Cargo pumps
 Number 8
 Type Submerged electrical centrifugal
 Make Ebara
 Material Aluminium alloy
 Capacity 8 x 1700m³/h
 Ballast control system
 Make Honeywell
 Type TPS (total plant solution)
 Complement
 Officers 13
 Crew 19
 Supernumeraries/spare 5
 Suez crew 6
 Rooms 35 x single; 1 x double; 1 x six
 Bow thruster
 Make Brunvoll
 Number 1
 Output 1600kW
 Bridge control system
 Make Kawasaki
 One man operation Yes
 Fire detection system
 Make Kongsberg
 Type BS-100 addressable
 Fire extinguishing systems
 Engine/room CO₂
 Make Unitor
 Cabins/public spaces Sea water and portable
 Make Unitor
 Radars
 Number 2
 Make KMSS (Kongsberg)
 Models Autocargo 2000
 Integrated bridge system
 Make KMSS (Kongsberg)
 Model Databridge 10
 Waste disposal plant
 Incinerator
 Make Teamtec
 Model GS500C
 Sewage plant
 Make Janghaph
 Model A-25
 Contract date 18 December 2000
 Launch/float-out date 31 August 2002
 Delivery date 17 June 2003

BERGE EVERETT





Barcelona Knutsen: 173,400m³ LNG carrier from Daewoo

Shipbuilder: **Daewoo Shipbuilding & Marine Engineering Co., Ltd**
 Vessel name: **Barcelona Knutsen**
 Hull No: **2267**
 Owner/Operator: **Knutsen OAS Shipping**
 Country: **Norway**
 Designer: **DSME**
 Country: **Norway**
 Model test establishment: **HSVA**
 Flag: **NIS**
 IMO number: **9401295**
 Total number of sister ships already completed (excluding ship presented): **0**
 Total number of sister ships still on order: **3**

BARCELONA Knutsen was delivered from Daewoo Shipbuilding and Marine Engineering Co. Ltd to Knutsen OSA Shipping, Norway on 10 February. The vessel has been designed and constructed to meet the requirements of Det Norske Veritas (DNV) with the class notation +1A1 of Liquefied Gas, Ship Type 2G(0.25bar -163°C, 500kg/m³), Nautilus(Newbuilding), Plus-2, E0, Naut-OC, F-A, CLEAN, Gas Fueled, RP, TMON, BIS. Four centre cargo tanks have a total capacity of 173,400m³ and have been designed by Gaz Transport & Technigaz (GTT) using its membrane system (GT NO 96 E-2) that will keep the liquefied natural gas (LNG) at a low temperature of -163°C with the maximum daily boil-off rate of less than 0.145% of fully loaded cargo volume.

Design fatigue life of hull structure is 40 years based on North Atlantic trading. The deck house is six tiers which is located aft of the vessel, providing accommodation for 46 persons including the Suez Crew. Care has also been taken in reducing the noise and vibration levels in this area.

The cargo handling systems onboard the *Barcelona Knutsen* have been designed to be capable of loading or discharging the LNG within 13 hours using eight cargo pumps with a capacity of 1900m³/h and four stripping/spray pumps. There is also vapour cargo handling equipment that comprises of two high duty compressors, two low duty compressors, one main vapouriser, one forcing vapouriser and one warm-up heater arranged in the cargo machinery room.

The bridge has been designed for optimum operational safety, efficiency and takes advantage of the current technology and rational navigational methods that are on the market. For one-man bridge operations the system is a modular workstation arrangement, meeting all design and equipment layout requirements in accordance with DNV's notation NAUT-OC.

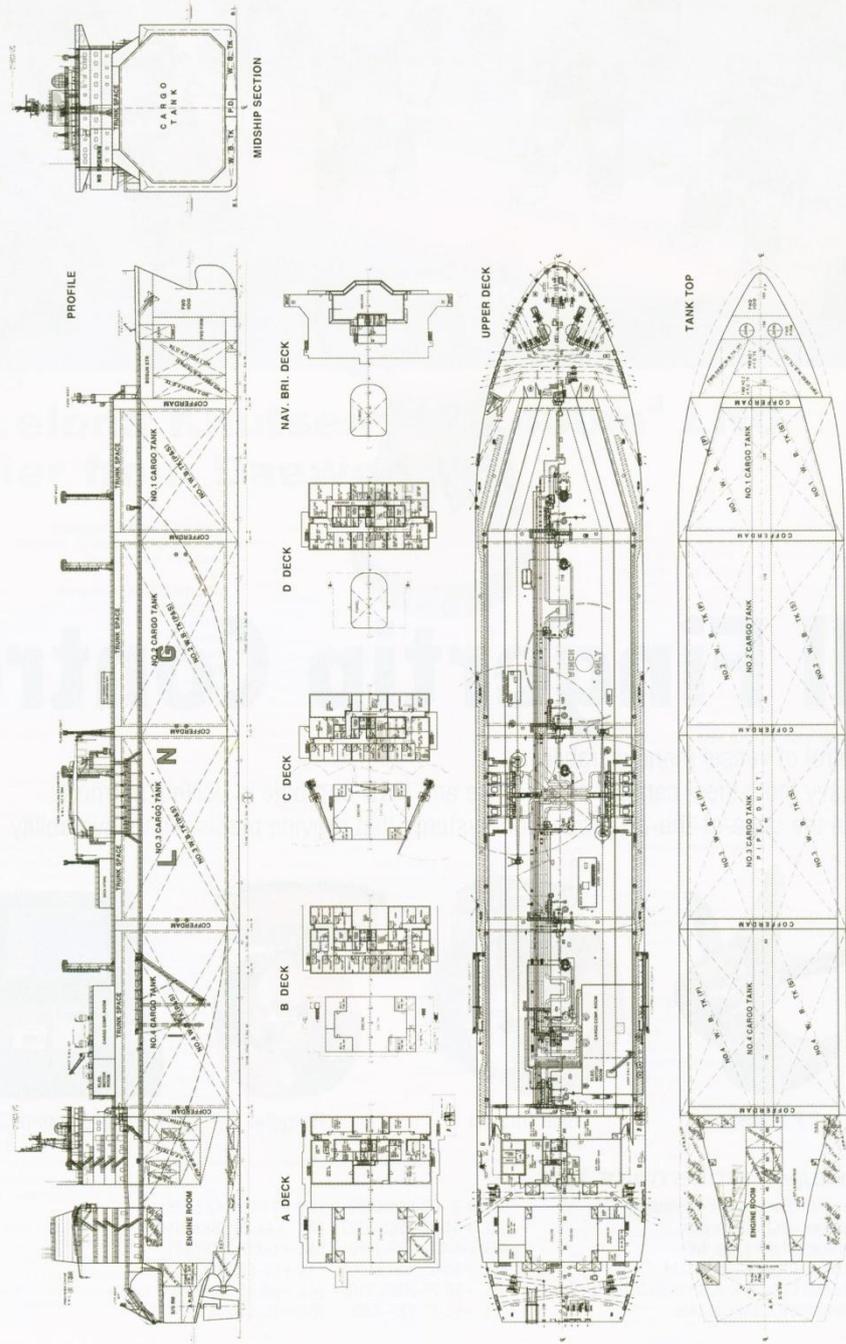
TECHNICAL PARTICULARS

Length oa: 290.0m
 Length bp: 279.0m
 Breadth moulded: 45.8m
 Depth moulded:

To upper decks: 26.5m
 Width of double skin
 Side: 2.21m
 Bottom: 3.2m
 Draught
 Scantling: 12.9m
 Design: 11.95m
 Gross: 110,920gt
 Displacement: 131,72tonnes
 Lightweight: 33,79tonnes
 Deadweight
 Design: 86,92dwt
 Scantling: 97,93dwt
 Block co-efficient: 0.778 @ scantling draught
 Speed, service: 19.5knots
 Cargo capacity
 Liquid volume: 173,650m³
 Bunkers
 Heavy oil: 5670m³
 Diesel oil: 530m³
 Water ballast: 57,86m³
 Daily fuel consumption
 Main engine only: 144.3tonnes/day
 Classification: DNV, +1A1, Tanker for Liquefied Gas, Ship type 2G(0.25bar, -163°C, 500kg/m³), NAUTICUS(Newbuilding), PLUS-2, E0, NAUT-OC, F-A, CLEAN, GAS FUELLED, RP, TMON, BIS.
 Main engines
 Design: Wartsila
 Model: 12V50DF x 3 sets
 9L50DF x 1 set
 Manufacturer: Wartsila
 Number: 4 sets
 Type of fuel: HFO/MDO/FUEL GAS
 Output of engine: 11,400kW x 3 sets
 8550kW x 1 set
 Gearboxes
 Make: Kawasaki Heavy Industries Ltd
 Model: M1H-190/67
 Number: 2 sets
 Output speed each: 13,240kW
 Propellers
 Material: Ni-Al-Bronze
 Designer/Manufacturer: DSME/Mecklenburger Metallguss GmbH
 Number: 2 sets
 Fixed/Controllable pitch: FPP
 Diameter: 7.8m
 Speed: 77.8m
 Special adaptations: Manufacturing tolerance - Class S of ISO 484/1 & Surface finish - Class S of ISO 484/1
 Main-engine driven alternators
 Number: 4 sets
 Make/Type: Convertam/M4HXD 253-71 x 3 sets, M4HXD 253-58 x 1 set/ self excited, brushless
 Output/Speed of each set: 11,000kW at 514rpm (M4HXD 253-71), 8250kW at 514rpm (M4HXD 253-58)
 Boilers
 Number: 2 sets

Type: Vertical water tube
 Make: Aalborg
 Output, each boiler: 6000kg/h
 Cargo cranes/cargo gear
 Number: 2
 Type: Dregen
 Type: Electro-hydraulic driven, single jib, cylinder luffing
 Performance: SWL 12tonnes
 Other Cranes
 Number: 2
 Make: Dregen
 Type: Electro-hydraulically driven, single jib, cylinder luffing
 Tasks: Provision and engine spare parts handling
 Performance: 12tonnes SWL
 Mooring equipment
 Number: 2
 Make: Rolls-Royce Marine
 Type: Hydraulic
 Special lifesaving equipment
 Number or each and capacity: 1 x 40 persons
 Make: Schat-Harding Equipment
 Type: Freefall launching type
 Cargo tanks
 Number: 4
 Cargo pumps
 Number: 8
 Type: Centri., vertical, submerged, single stage, direct built-in el-motor driven
 Make: Shinko Industries Ltd
 Capacity: 1900m³ x 160mL/C
 Cargo control system
 Make: Emerson
 Type: Radar beam type for cargo tank level gauging
 Ballast control system
 Make: Hanla IMS
 Type: Electro-Pneumatic
 Complement
 Officers: 19
 Crew: 21
 Suez/Repair crew: 6
 Fire detection system
 Make: Autonica fire and safety
 Type: Autosale
 Fire extinguishing systems
 Cargo holds: Wilhelmsen/Dry powder
 Engine room: Wilhelmsen/ High Exp. Foam system
 Radars
 Number: 2
 Make: JRC
 Model: JMA-9132-SA, JMA-9122-6XA
 Waste disposal plant
 Incinerator: Teamtec GS500CS
 Waste compactor: Metos IMCIP400
 Sewage plant: Evac JMC-BIO AEROB-18
 Contract date: 29 June 2006
 Launch/float-out date: 16 May 2009
 Delivery date: 10 February 2010

BARCELONA KNUTSEN





BRITISH EMERALD: LNG tanker with dual-fuel/diesel-electric propulsion

Shipbuilder: Hyundai Heavy Industries Co Ltd, (HHI), Korea
British Emerald
 Hull number: 1777
 IMO number: 9333591
 Owner: BP Shipping Ltd, UK
 Designer: Hyundai Heavy Industries Co Ltd, Korea

Model test establishment used: SSPA, Sweden
 Flag: Isle of Man
 Total number of sister ships already completed: Nil
 Total number of sister ships still on order: 5

BRITISH Emerald's reign as the largest LNG carrier in the world, at 155,000m³, was short-lived (as can be seen by other entrants in this year's *Significant Ships*); nevertheless, this lead vessel of BP's new Gem class is of special interest because of its 'green' credentials, and for introducing - for this owner - an innovative propulsion system (the first dual-fuel/diesel LNG tanker was *Gaz de France Energy*, presented in our 2004 review). The use of dual-fuel marine engines is not new, but its combination here in a diesel-electric configuration (DFDE) brings a new dimension into the selection of gas-ship machinery, previously dominated by the steam turbine.

The machinery installation here is centred on four Wärtsilä type 50DF main engines: two 12-cylinder vee-type units and two with nine cylinders in line, of 11,400kW and 8550kW output, which are connected, respectively, to Convertteam alternators producing 11,000kW/8250kW. These are, perhaps uniquely, each positioned directly above the propulsion motors in the two engine rooms included for redundancy purposes, and supply the ship's main electrical requirements, as well as powering two 14,860kW propulsion motors, connected via a Renk twin-input/single-output reduction gearbox to a five-bladed propeller producing a service speed of 20knots.

The main engines can operate on conventional diesel fuel or, on a loaded voyage, on boil-off gas from the cargo which is heated up and delivered as fuel gas by low duty compressors. Comparison between DFDE and similar steam-propelled gas carriers is understood to show that the latter, burning oil and gas, produced 530tonnes of CO₂ and 7tonnes SOx daily, whilst the DFDE vessel, burning only gas, emitted just 386tonnes of CO₂.

British Emerald has a flat, single-deck, with sunken mooring deck aft, and a double-skin hull containing four membrane-type cargo tanks separated by cofferdams, and constructed in accordance with the GTT Mk III containment system for carrying cargoes at cryogenic temperatures of -163°C. Tank insulation is 270mm thick to satisfy a low boil-off rate of 0.15% by volume of total cargo per day. The tanks extend above the upper deck and are enclosed in a trunk which

provides access passages fore and aft.

A shore manifold is arranged P&S between tanks 2 and 3 and a compressor room is situated on the starboard side of the trunk. Cargo is loaded by shore pumps, with unloading handled by having two Ebara 1800m³/h electric, submerged pumps in each tank.

Other features included in the specification are the new technology of 'cold ironing' facilities to allow the vessel to accept shore power whilst in port, and the application of external paint colours proven to reduce solar energy absorption, resulting in less natural heating of cargo and consequently minimising production of boil-off gases.

TECHNICAL PARTICULARS

Length, oa	260.00m
Length, bp	275.00m
Breadth, moulded	44.20m
Depth, moulded to main deck	26.00m
to trunk deck	33.09m
Width of double skin side	2.76m
bottom	3.20m
Draught design	11.47m
scantling	12.20m
Gross	102,000gt
Deadweight design	76,600dwt
scantling	84,300dwt
Speed, service, MCR with 15% sea margin	20knots
Cargo capacity, liquid volume	155,000m ³
Bunkers heavy oil	nil
diesel oil	6600m ³
Water ballast	59,000m ³
Fuel consumption (diesel oil equivalent)	143.3tonnes/day
Liquefied Gas Tanker, Ship Type 2G, SG 0.5, 0.25bar g, -163°C, *IWS ShipRight(SDA), L1, EP, +LMC, UMS, ICC, NAV	
Percentage of high tensile steel used in construction	approx 2%
Dual fuel diesel electric (DFDE) power system	
Main engines Design	Wärtsilä
Number/models	2 x 12V50DF/2 x 9L50DF
Manufacturer	Wärtsilä
Type of fuel used	Boil-off gas/MDO
Output, each engine	2 x 11,400kW/2 x 8550kW
Alternators Number	4
Make	Convertteam
Output, each unit	2 x 11,000kW/2 x 8250kW
Propulsion motors Number	2
Make	Convertteam
Output, each unit	2 x 14,860kW

Frequency converters Number/type	2/synchronous
Make	Convertteam
Gearbox Make	Renk
Number	1
Model	NDSH-4000 (twin input/single output)
Output speed	720 rev/min (input)/90.6rev/min (output)
Propeller Material	Nickel-aluminium-bronze
Designer/Manufacturer	Hyundai
Number	1
Pitch	Fixed
Diameter	8600mm
Speed	90.6rev/min
Boiler Number	1
Make	KangRim Heavy Industries
Output	15,000kg/h
Cargo tanks Number	4
Grades of cargo carried	LNG
Cargo pumps Number	8
Type	Vertical, submerged, centrifugal
Make	Ebara
Material	Stainless steel
Capacity	8 x 1800m ³ /h
Ballast/cargo control systems Make	Convertteam
Type	Integrated automation system
Complement Officers	22
Crew	11
Suez/repair crew	6
Bow thruster Number	1
Make	Brunvoll
Output	2000kW
Bridge control system Make	Furuno
One man operation	Yes
Fire detection system Make/type	Consilium CS 3000
Fire extinguishing systems Cargo area	Unitor/dry powder
Engine room	Unitor/high-pressure CO ₂
Radars Number/make	2 x Furuno
Models	FAR-2637SW/ FAR-2627W
Inclinerator Make/type	Hyundai/MAXI 150SL-1 WS
Sewage plant Make/type	Jonghap/BIO AEROB-25
Contract date	April 2004
Launch/float-out date	July 2006
Delivery date	5 July 2007



BRITISH TRADER: advanced LNG tanker

Shipbuilder:..... Samsung Heavy Industries Co Ltd, Korea
 Vessel's name:..... *British Trader*
 Hull number:..... 1380
 Owner/operator:..... BP Shipping, UK
 Designer:..... Samsung Heavy Industries Co Ltd, Korea
 Model test establishment used:..... SSPA, Sweden
 Flag:..... Isle of Man
 Total number of sister ships already completed:..... Nil
 Total number of sister ships still on order:..... 2

BRITISH TRADER has been constructed in accordance with the Gaz Transport & Technigas Mark III cargo containment system for the carriage of LNG cargoes at cryogenic temperature (-163°C) and atmospheric pressure. Within a double hull, which has been designed to last for a period of not less than 40 years, there are four cargo tanks, encased in a primary membrane of 1.2mm-thick corrugated, SUS 304L grade, stainless steel plates, and a secondary membrane of triplex glass wool. Insulation is made up of 270mm reinforced polyurethane foam, and the system allows the daily boil-off gas rate to be restricted to 0.15% of the total cargo volume.

Two 1700m³/h cargo pumps are fitted in each tank, capable of completely discharging the cargo in 12 hours, following pre-cooling by LNG spray. Two 8000m³/h, low-duty, and two 26,000m³ high-duty compressors are installed, together with four spray pumps: a 550m³/h emergency cargo pump, two warming-up heaters, an LNG vaporiser, forcing vaporiser, a 14,000Nm³/h inert-gas generator and two 90Nm³/h nitrogen generators.

The machinery installation is centred on a Kawasaki cross-compound steam turbine, supplied with steam from boilers which burn fuel oil or boil-off gas, or a combination of both. This drives a six-bladed propeller for a service speed of 20.10knots. Electrical power is produced by two 3450kW steam-turbine driven alternators, with a similar-sized diesel set as stand-by. A 2500kW thruster is fitted at the bow.

British Trader is equipped with a 'centralised administration and control centre', with integrated automation system (IAS) and shipboard management

system (SMS), which serves as a central command station for carrying out cargo and ballasting operations, and monitoring and remotely controlling the propulsion plant. Also installed is a one-man bridge system complying with Lloyd's Register's NAV1/IBS notation, an ECDIS, a manoeuvring simulator, GMDSS console, voyage data recorder, and automatic identification system.

Other features of note included in the specification are a ballast water exchange system which uses sequential empty/refill procedures to complete the operation in under 30hours. The diesel-alternator engine has a low NOx emission, and there is an emergency operation for water ballast leakage, a CO₂ blowing agent for the insulation system, and all paint complies with environmental requirements.

TECHNICAL PARTICULARS

Length, oa..... 278.80m
 Length, bp..... 266.00m
 Breadth, moulded..... 42.60m
 Depth, moulded.....
 to main deck..... 26.00m
 to trunk deck..... 32.70m
 Width of double skin.....
 side..... 2.30m
 bottom..... 3.40m
 Draught.....
 design..... 11.35m
 scantling..... 12.30m
 Air draught (approx)..... 50.00m above base
 Displacement, at 12.30m..... 107,300tonnes
 Lightweight..... 29,800tonnes
 Deadweight.....
 design..... 68,100dwt
 scantling..... 77,500dwt
 Speed, service..... 20.10knots at 85% MCR with 15% sea margin
 Cargo capacity.....
 liquid volume..... 138,200m³
 Bunkers.....
 heavy oil..... 7700m³
 diesel oil..... 400m³
 Water ballast..... 54,800m³
 Fuel consumption..... 170.90tonnes/day
 Classification..... Lloyd's Register of Shipping +100A1 Liquefied Gas

Tanker, Ship Type 2G, Methane (LNG) in Membrane Tanks. Maximum vapour pressure 0.25bar, minimum temperature minus 163°C/ ShipRight (SDA), IWS, L1, + LMC, UMS, CCS, ICC, NAV1, IBS, with descriptive notes ShipRight (FDA, CM, HCM, SEA(HSS-4), SEA (VDR-4), PMS(CM), SCM), Part high-tensile steel, ETA Percentage of high-tensile steel used in construction..... 2.3%

Steam turbine.....
 Design..... Cross-compound impulse turbine
 Manufacturer..... Kawasaki Heavy Industries
 Number..... 1
 Output..... 39,500shp MCR/33,580shp NCR at 85.3rev/min

Gearbox.....
 Make..... Kawasaki Heavy Industries
 Model..... UA-400
 Number..... 1
 Output speed..... 90rev/min MCR

Propeller.....
 Manufacturer..... Mitsubishi Heavy Industries
 Number..... 1
 Pitch..... Fixed
 Diameter..... 8250mm
 Speed..... 90rev/min MCR

Steam-turbine driven alternators.....
 Number..... 2
 Make/type..... Shinko/multi-stage
 Output..... 2 x 3450kW/1800rev/min

Diesel-driven alternator.....
 Number..... 1
 Engine make..... Wärtsilä
 Output/speed..... 3600kW/720rev/min
 Alternator make..... ABB
 Output/speed..... 3450kW/720rev/min

Boilers.....
 Number..... 2
 Type..... Water tube, forced draught
 Maker..... Kawasaki Heavy Industries
 Output..... 2 x 65tonnes/h

Mooring equipment.....
 Make..... Kocks
 Type..... Self-contained hydraulic

Cargo tanks.....
 Number..... 4
 Structure and piping..... Stainless steel

Cargo pumps.....
 Number..... 8
 Type..... Submerged electric
 Make..... Ebara International
 Capacity..... 8 x 1700m³

Cargo and bridge control systems.....
 Type..... Integrated with IAS

Complement.....
 Officers..... 22
 Crew..... 11
 Suez/repair crew..... 6

Bow thruster.....
 Make..... Kawasaki Heavy Industries
 Number..... 1
 Output..... 2500kW

Fire detection system.....
 Make..... Consilium
 Type..... Analogue addressable

Fire extinguishing system.....
 On deck..... Dry powder
 Make..... NK
 Engine room..... CO₂
 Cabins/public spaces..... Sea water

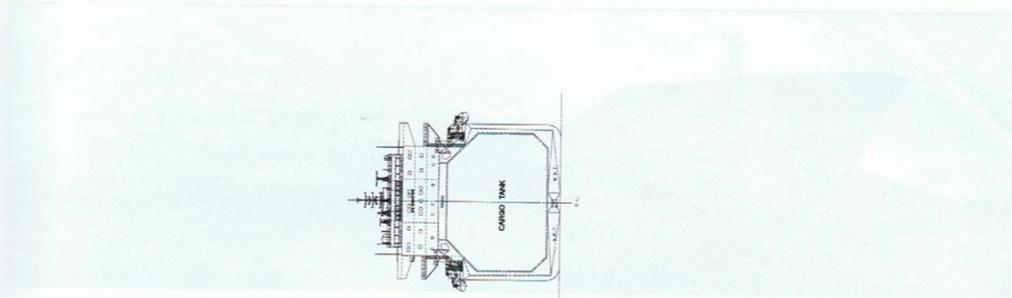
Radars.....
 Number..... 2
 Make..... Kongsberg
 Model..... 2 x DB10

Satellite navigation systems.....
 Number..... 2 x DGPS
 Make..... Leica
 Model..... MX412

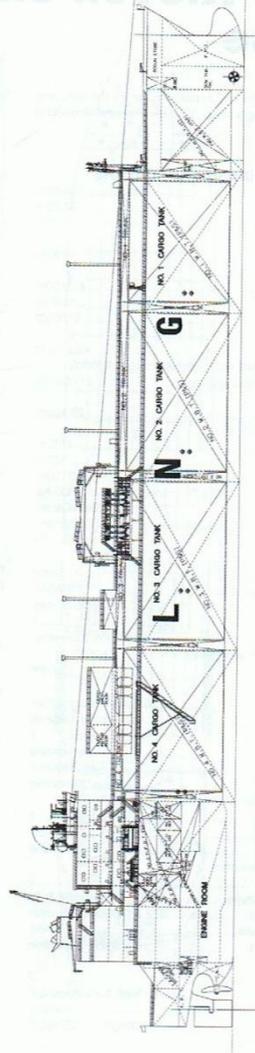
Waste disposal systems.....
 Incinerator.....
 Make..... TeamTec
 Model..... OGS400C
 Waste compactor.....
 Make..... Hackman Metos
 Model..... Orwak 5030
 Waste shredder/crusher.....
 Make..... Bin Systems
 Model..... F515

Contract date..... 20 July 2000
 Launch/float-out date..... 9 December 2001
 Delivery date..... 15 November 2002

BRITISH TRADER



CARLOS FISCHER: Kieven extends its fruit juice expertise





CASTILLO DE SANTISTEBAN: STX LNG carrier with extra cargo tank capacity

Shipbuilder: **STX Offshore & Shipbuilding Co., Ltd**
Castillo De Santisteban
 Hull No: **S3008**
 Owner/Operator: **Empresa Naviera Eicano SA**
 Country: **Spain**
 Designer: **STX Offshore & Shipbuilding Co., Ltd**
 Country: **Korea**
 Model test establishment used: **MOERI/SSPA**
 Flag: **Malta**
 IMO number: **9433717**
 Total number of sister ships already completed (excluding ship presented): **0**
 Total number of sister ships still on order: **0**

STX Offshore & Shipbuilding delivered its liquefied natural gas (LNG) carrier, *Castillo De Santisteban*, to Empresa Naviera Eicano SA in August. The vessel has the defining feature of having a maximum tank size that is accepted by Gaz Transport & Technigaz (GTT) with a No 93E2 membrane cargo system.

The hull of *Castillo De Santisteban* is divided into four cargo tanks by cofferdams that are built between cargo tanks and consist of five pairs of water ballast tanks in the side and bottom space.

The cargo containment, handling, control and measuring systems are designed and constructed to transport liquefied natural gas in four membrane cargo tanks at about -163°C and at the absolute pressure of 106kPa. The water ballast carried in tanks which are coated in epoxy A/C is handled by three 3300m³ pumps installed on the double bottom in E/R.

The additional Bureau Veritas (BV) class notation SYS-NEQ is assigned to ships which are fitted with a centralised navigation control system so arranged that the navigation and manoeuvring of the ship can be operated under normal conditions by one person, for periodical one man watch. The notation includes specific requirements for prevention of accidents.

The main propulsion consists of main dual-fuel generator engines and propulsion motors with reduction gear driving a single screw propeller through the main shafting.

The propulsion system is a dual fuel diesel electric, capable of burning a combination of natural and forced boil off gas. The power generating plant utilises all available natural boil off gas and makes up the required power by consuming additional forced boil off gas. The electric generators consist of five MAN 8L51/60DF main generators, one turbo generator, which generates electricity using waste heat gas making for a 5% fuel saving and one emergency diesel generator. *Castillo De Santisteban* also has a DF boiler and heel-out operation mode reducing gas waste and increasing the efficiency of the vessel.

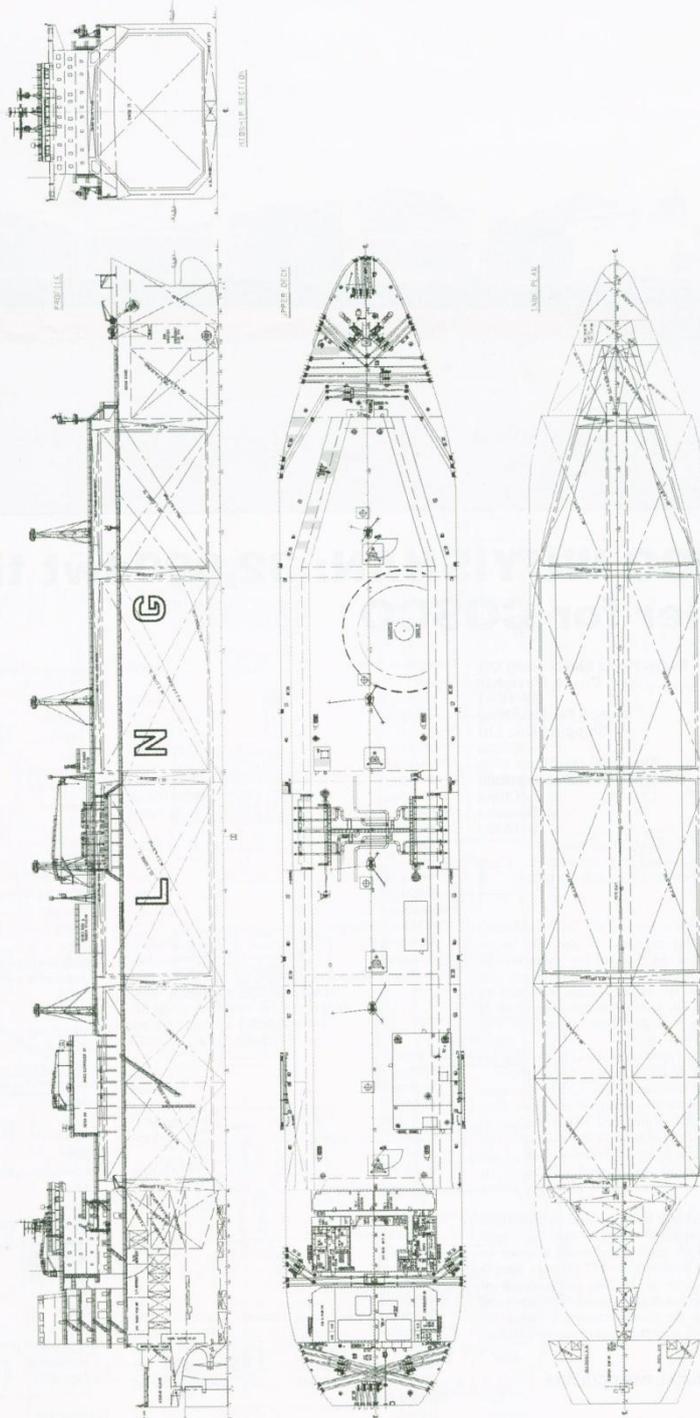
TECHNICAL PARTICULARS

Length oa: 199.90m
 Length bp: 288.00m

Breadth moulded: 45.80m
 Depth moulded:
 To main deck: 26.00m
 To upper deck: 26.00m
 To other decks: 33.55m
 Width of double skin
 Side: 2.39m
 Bottom: 3.20m
 Draught
 Scantling: 12.50m
 Design: 11.60m
 Gross: 111,665gt
 Displacement: 128,987tonnes
 Deadweight: 83,515dwt
 Scantling: 93,796dwt
 Block co-efficient: 0.7614
 Speed, service: 20.42knots
 Cargo capacity
 Liquid volume: 173,887m³
 Bunkers
 Heavy oil: 5616m³
 Diesel oil: 559m³
 Water ballast: 61,244m³
 Daily fuel consumption
 Main engine only: 0
 Auxiliaries: 143.5tonnes/day
 Classification society and notations: Bureau Veritas I+Hull, +Mach, Unrestricted Navigation, Liquefied Gas Carrier, +Veristar-Hull, DFL 40 Years, +AUT-UMS, AUT-CCS, AUT-PORT, SYS-NEQ-1, Inwatersurvey, MON-Shaft
 % high-tensile steel used in construction: less than 10%
 Gearbox
 Make: Kawasaki
 Model: M2H-400/85
 Number: 1
 Output speed: 84.9rpm
 Propellers
 Material: Ni-Al-Bronze
 Designer/Manufacturer: Hyundai Heavy Industries
 Number: 1
 Fixed/Controllable pitch: Fixed pitch
 Diameter: 8700mm
 Speed: 84.9rpm
 Diesel-driven alternators
 Number: 5
 Engine make/type: MAN Diesel/ 8L51/60DF
 Type of fuel: BOG, MDO, HFO
 Output/speed of each set: 8000kW x 514rpm
 Alternator make/type: ABB
 Output/speed of each: 7700kW x 514rpm
 Boilers
 Number: 2
 Type: Oil fired + oil fired and gas fired
 Make: Aalborg
 Output, each boiler: 16tonnes x 8.5bar
 8tonnes x 3.5bar
 Cargo cranes/cargo gear
 Number: 2
 Make: Oriental Precision & Engineering
 Type: Electro-hydraulic cylinder luffing, Single jib arm
 Performance: 15tonnes x 25m SWL

Other cranes
 Number: 2
 Make: Oriental Precision & Engineering
 Type: Electro-hydraulic, single jib arm
 Tasks: Provision crane
 Performance: 10tonnes x 10m SWL
 10tonnes x 6m SWL
 Mooring equipment
 Number: 10
 Make: Rolls-Royce
 Type: Hydraulic
 Special lifesaving equipment
 Number of each and capacity: 2 x 48 persons
 Make: Hyundai liferaft
 Type: Totally enclosed type
 Cargo tanks
 Number: 4
 Product range: Liquefied natural gas
 Coated tanks: Cargo containment system with Invar membrane
 Cargo pumps
 Number: 8
 Type: Vertical, submerged
 Make: Shinko
 Stainless steel: Al Alloy casting
 Capacity: 2050m³/h at 160mic
 Cargo control system
 Make: Kongsberg
 Type: K-Chief 700
 Ballast control system
 Make: Kongsberg
 Type: K-chief 700
 Complement
 Officers: 21
 Crew: 17
 Suez/Repair crew: 6
 Bow thrusters
 Make: Kawasaki Heavy Industries
 Number: 1
 Output: 2000kW
 Bridge control system
 Make: ABB
 Type: OS800
 One-Man operation: Yes
 Fire detection system
 Make: Consilium
 Type: CS4000
 Fire extinguishing systems
 Cargo holds: Wilhelmsen Dry powder, sea water
 Engine room: Wilhelmsen High expansion foam
 Cabins: Sampo Eng. Galley hood fire fighting system
 Public spaces: NK CO₂ fire extinguishing system
 Radars
 Number: 2
 Make: Furuno
 Model: FAR-2827 (x-Band), FAR-2837S (S-Band)
 Integrated bridge system
 Make: Furuno
 Model: FEA-2107
 Contract date: February 2007
 Launch/float-out date: April 2009
 Delivery: August 2010

CASTILLO DE SANTISTEBAN





DAPENG SUN: first Chinese-built LNG carrier

Shipbuilder: **Hudong-Zhonghua Shipbuilding (Group) Co Ltd (China State Shipbuilding Corp), People's Republic of China**
 Vessel's name: **Dapeng Sun**
 Hull number: **H1308A**
 IMO number: **9308479**
 Owner/technical manager: **Yue Peng LNG Shipping Co Ltd, Hong Kong/China LNG Shipping (International) Co Ltd (CLSICO), Hong Kong**
 Flag: **Hong Kong**
 Total number of sister ships already completed: **Nil**
 Total number of sister ships still on order: **4**

DAPENG SUN is another product of the burgeoning Hudong-Zhonghua Shipyard in Shanghai but this ship's most notable claim to fame is as the first LNG carrier to be built in China. It is the lead ship of a series of five, constructed in collaboration with the former Alstom Atlantique shipyard at St Nazaire (now operating as part of STX Europe), one of the pioneers of large-capacity LNG carrier construction.

Destined for operation between the North West Shelf LNG export facility at Withnell Bay, near Dampier in Western Australia, and China's first gas receiving terminal at Dapeng, Guangdong province, the vessel has entered service with a complex joint venture ownership network, involving participants in the North West Shelf project, COSCO Dalian, the Chinese LNG industry, and Hong Kong based shipowners. Shell International carried out shipyard supervision, and the technical management company (CLSICO) includes BP Shipping in its organisation.

Cargo is carried in four tanks contained within a complete double side/bottom/bulkhead structure with topside tanks, the inner line of which is carried up to form the side of a nearly full length upper deck trunk. Gas is transported at temperatures of -163°C and at near atmospheric pressure using a GTT NO96 containment system. This has primary and secondary membranes formed of Invar (36% nickel steel), in conjunction with other proven insulation materials to satisfy the required boil-off rate.

All cargo system components are subject to cryogenic temperatures, and handling is carried out using eight (two per tank) electric, stainless steel, submerged pumps each with a capacity of 1500m³/hour, and supplied from Spain by Ebara, along with four 50m³/hour spray pumps. Cargo and ballast operations are controlled by a Centrum CS3000 integrated automation system

installed by the Yokogawa Electric Corp.

Dapeng Sun is fitted with a steam turbine machinery plant consisting of a UA-400 high pressure/low pressure set, including a cross compound, tandem articulated, double reduction gearbox, all supplied by Kawasaki. Mitsubishi provided two type MB-4E-KS2 water tube, internally superheated boilers, burning either HFO, low-sulphur grade HFO, or boil-off gases from the cargo to supply the turbine, which develops 27,300kW at 83rev/min. Service speed is recorded at 19.50knots at MCR, using a Mecklenburger Metallguss fixed pitch propeller.

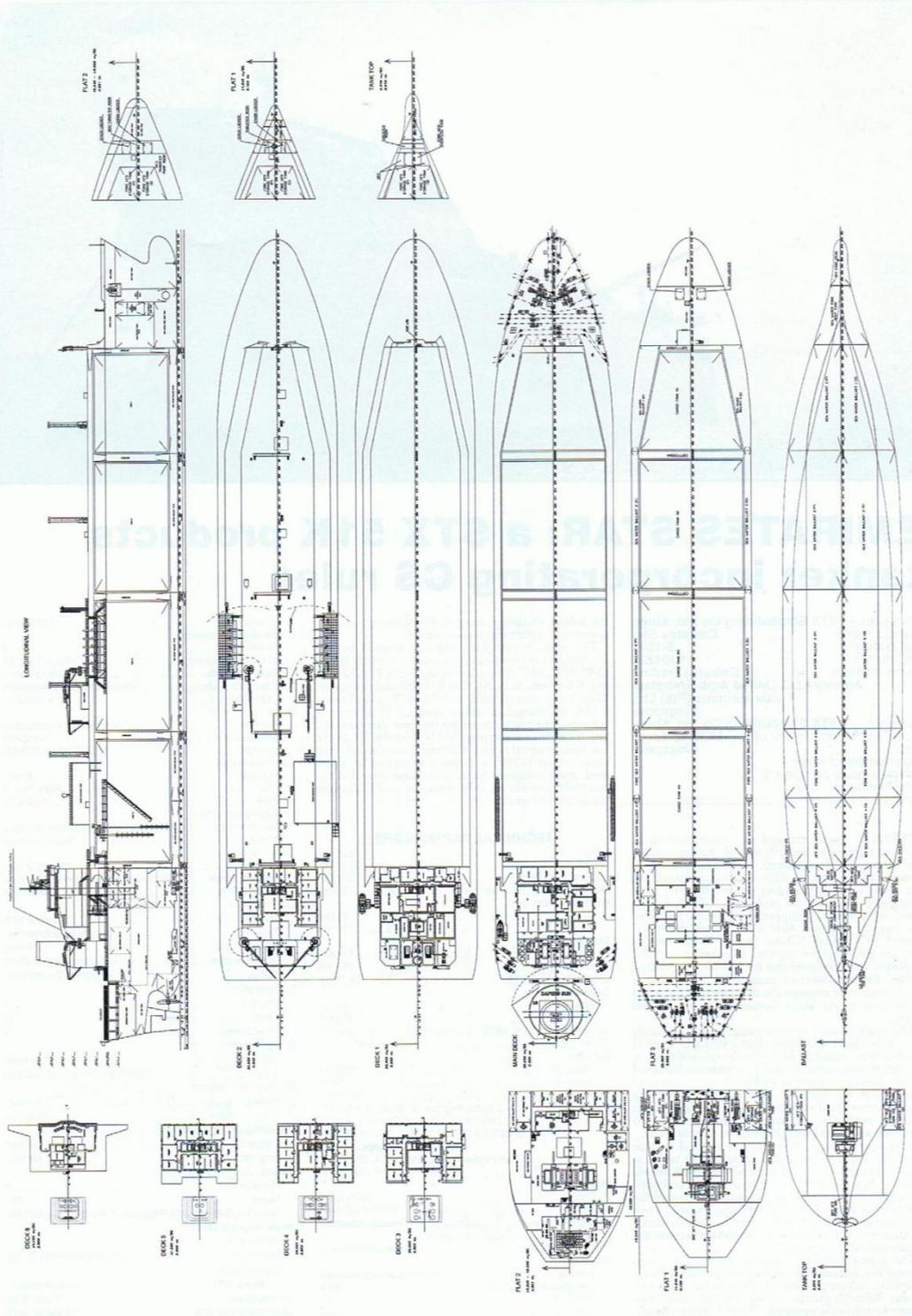
Electrical supply comes from two Mitsubishi/ABB steam turbine-driven alternator sets each producing 3200kW at 1800rev/min. Two 2000kVA ABB alternators, driven by MAN diesel engines running on MDO, are also fitted. Enhancing manoeuvrability is a Kawasaki 2000kW bow thruster.

TECHNICAL PARTICULARS

Length, oa 292.00m
 Length, bp 274.10m
 Breadth, moulded 43.35m
 Depth, moulded 26.25m
 Draught
 design 11.45m
 scantling 12.33m
 Gross 97,871gt
 Lightweight 31,739tonnes
 Deadweight
 design 83,050dwt
 Speed, service, MCR 19.50knots
 Cargo capacity 147,237m³ (100% full)
 Bunkers
 heavy oil 5011m³
 heavy oil (low sulphur) 490m³
 diesel oil 323m³
 Water ballast 54,762m³
 Classification American Bureau of Shipping +A1 (E), Liquefied Gas Carrier, Ship Type ZG, Membrane Type 0.23bar, -163°C, 500kg/m², SH-DLA, SH-RL(40), SFA (40), SHCM, UWILD, +AMS, +ACCU, NBLES, HM3-R, ES & equivalent of LR LI, SCM, TCM, BWMP
 Main engine
 Design Steam turbine
 Model Kawasaki UA-400
 Manufacturer Kawasaki Heavy Industries
 Number 1
 Type of fuel used HFO/LNG (boil off)
 Output 27,300kW/83rev/min
 Gearbox
 Make Kawasaki
 Type Cross compound, tandem articulated, double reduction
 Propeller
 Material phosphor bronze
 Manufacturer Mecklenburger Metallguss
 Number 1
 Pitch Fixed

Diameter 8800mm
 Speed 83rev/min
 Steam turbine-driven alternators
 Number 2
 Turbine make/type Mitsubishi/AT420T-B
 Alternator make/type ABB/
 Output 2 x 3200kW/6600V
 Diesel-driven/alternators
 Number 2
 Engine make MAN
 Type of fuel used MDO
 Alternator make/type ABB/
 Output 2 x 2000kVA/6600V
 Boilers
 Number 2
 Make/type Mitsubishi/MB-4E-KS2
 Output 2 x 65,000kg/h
 Mooring equipment
 Number 2 x winlass; 8 x mooring winch
 Make
 Type Electric
 Cargo tanks
 Number 4
 Grades of cargo LNG
 Containment system GTT NO96 with Invar
 Cargo pumps
 Number 8
 Type Electric, submerged
 Make Ebara International Corp
 Stainless steel Yes
 Capacity 8 x 1500m³/h
 Ballast/cargo control systems
 Make Yokogawa Electric Corp
 Type Centrum CS3000 integrated automation system
 Complement
 officers 19
 crew 13
 Bow thruster
 Make Kawasaki
 Number/type 1 x KT 219B
 Output 2000kW/270rev/min
 Bridge control system
 Make Furuno
 Type Integrated bridge system
 One man operation Yes
 Fire detection system
 Make Autronica
 Type Release 3 interactive fire alarm
 Fire extinguishing systems
 Cargo area Unitor dry powder
 Engine room Unitor Hi-Foam/Mariott water spray
 Radars
 Number 2
 Make Furuno
 Models FAR 2827W; FAR288837SW
 Waste disposal plant
 Incinerator Deerberg Delta IRL-50
 Sewage plant Hamworthy SA4A
 Contract date 11 August 2004
 Launch/float-out date 28 December 2005
 Delivery date 3 April 2008

DAPENG SUN



EXCELSIOR



EXCELSIOR: first re-gasifying LNG carrier for the Energy Bridge concept

Shipbuilder: Daewoo Shipbuilding & Marine Engineering Co Ltd, (DSME), Korea
 Vessel's name: *Excelsior*
 Hull number: 2208
 Owner/operator: Exmar NV, Belgium
 Designer: DSME, Korea
 Model test establishment used: SSPA, Sweden
 Flag: Belgium
 Total number of sister ships already completed: Nil
 Total number of sister ships still on order: 2

ENERGY BRIDGE is the name given to an innovative concept introduced by Exmar, Excellerate Energy, and DSME, which allows a tanker, having loaded an LNG cargo in the conventional way, to re-gasify the cargo on board and discharge the high-pressure gas, at an offshore buoy or floating terminal. Gas is then fed directly into the consumer grid system through a dedicated mooring arrangement and sub-sea pipeline, thereby by-passing the need for a costly shore terminal which would normally carry out this process.

The so-called 'LNG re-gasification (re-gas) vessel (LNG RV)' has been developed by DSME from its standard 138,000m³ capacity LNG tanker design (*Berge Everett*, *Significant Ships of 2003*), to which has been added regas facilities and an internal turret for sub-sea pipe connection and weather-vane mooring. That basis vessel featured a double hull containing four prismatic cargo tanks separated by cofferdams. They extended through the upper deck to form a trunk, and were constructed in accordance with the conventional GTT NO96 membrane containment system.

This has been retained, but, because the LNG RV will be operating under partially filled tank conditions involving cargo sloshing, especially when moored to a buoy, it, and the supporting structure, has been significantly reinforced in the new ship. Cargo handling in the LNG mode also remains as before, using eight submerged 1700m³/h electric pumps mounted in pump tower masts in the four tanks and capable of discharging a full liquid cargo in 12 hours: high- and low-duty compressors, main and forcing vaporisers, and boil off/warm up heaters are also included in the system.

For the LNG RV role, additional equipment has been provided, with three 620m³/h feed pumps in tanks 2, 3 and 4 supplying a re-gas process, comprising six sets of 205m³/h high-pressure pumps and vaporisers, arranged

three each, port and starboard, above No 1 tank. The normal re-gasification capacity is 500mm³/sd (500 million standard cubic feet per day), ensuring that a full 138,000m³ cargo can be converted to high-pressure natural gas in five-to-six days.

Discharge is effected either through P&S deck manifolds or, more particularly, in line with the Energy Bridge concept, via a submerged turret mooring and offloading (STL) system, employing a turret installed at the bow. A buoy is moored to the sea bed at the terminal and this is pulled into, and secured to, the turret's mating cone in the ship's bottom. A swivel in the turret allows the ship to weathervane without the aid of propulsion, and a quick-release feature is installed. During normal LNG transfer, the re-gas plant is depressurised, inerted, and segregated from the normal cargo piping.

Accurate manoeuvring and positioning at the STL mooring buoy is a necessary component of the operation, and a differential GPS system has been installed which can place the mating cone within some 2m of the buoy. Assisting this manoeuvre is an acoustic position-reference system (APRS), using acoustic transceivers and transponders to monitor the buoy position. Two 1500kW bow thrusters, and one 2000kW stern unit, are also installed.

A Kawasaki 26,650kW steam turbine propulsion unit is fitted, supplied by two boilers burning fuel oil or boil-off gas. Three 3600kW steam turbine-driven generators and a 3700kW diesel set (all slightly larger than on *Berge Everett*) satisfy electrical requirements.

TECHNICAL PARTICULARS

Length, overall	277.00m
Length, bp	266.00m
Breadth, moulded	43.40m
Depth moulded	
to upper deck	26.00m
to surken mooring deck, aft	21.26m
Width of double skin	
side	2.21m
bottom	3.20m
Draught	
design	11.50m
scantling	13.20m
Gross	93,800gt
Deadweight	
design	68,130dwt
scantling	76,130dwt
Speed, service, 90% MCR, 21% sea margin	19.10knots
Cargo capacity	138,000m ³
Bunkers	
heavy oil	5700m ³
diesel oil	350m ³
Water ballast	51,000m ³

Fuel consumption, main engine only 170tonnes/day
 Classification Bureau Veritas 1 + Hull, + Mach, Liquefied Gas Carrier, Ship type 2G (Membrane tank, 0.25bar, -163°C, 500kg/m³), Unrestricted Navigation, + VeniSTAR-Hull, + AUT-UMS, +SYS-NEQ-1, SPM/STL, IWS

Steam turbine
 Design Kawasaki Heavy Industries
 Model UA-360
 Number 1
 Type of fuel used HFO and boil-off gas
 Output/speed 26,650kW/88rev/min

Propeller
 Designer/manufacturer
 Material Nickel-aluminium-bronze
 Number 1
 Pitch Fixed
 Speed 88rev/min

Steam turbine-driven alternators
 Manufacturer
 Number 3
 Output, each set 3600kW

Diesel-driven alternator
 Manufacturer, diesel engine
 Manufacturer, alternator
 Number 1
 Output 3700kW

Boilers
 Number 2
 Manufacturer
 Type vertical, two-drum water tube
 Output 2 x 68,000kg/h

Mooring equipment
 Number 9 x mooring winch
 Lifesaving equipment
 Number/type 2 x 40-person lifeboats, totally enclosed

Cargo tanks
 Number 4
 Grades of cargo carried LNG

Cargo pumps
 Manufacturer
 Number 8
 Type Submerged electric centrifugal
 Shaft stainless steel
 Capacity, each pump 1700m³/h

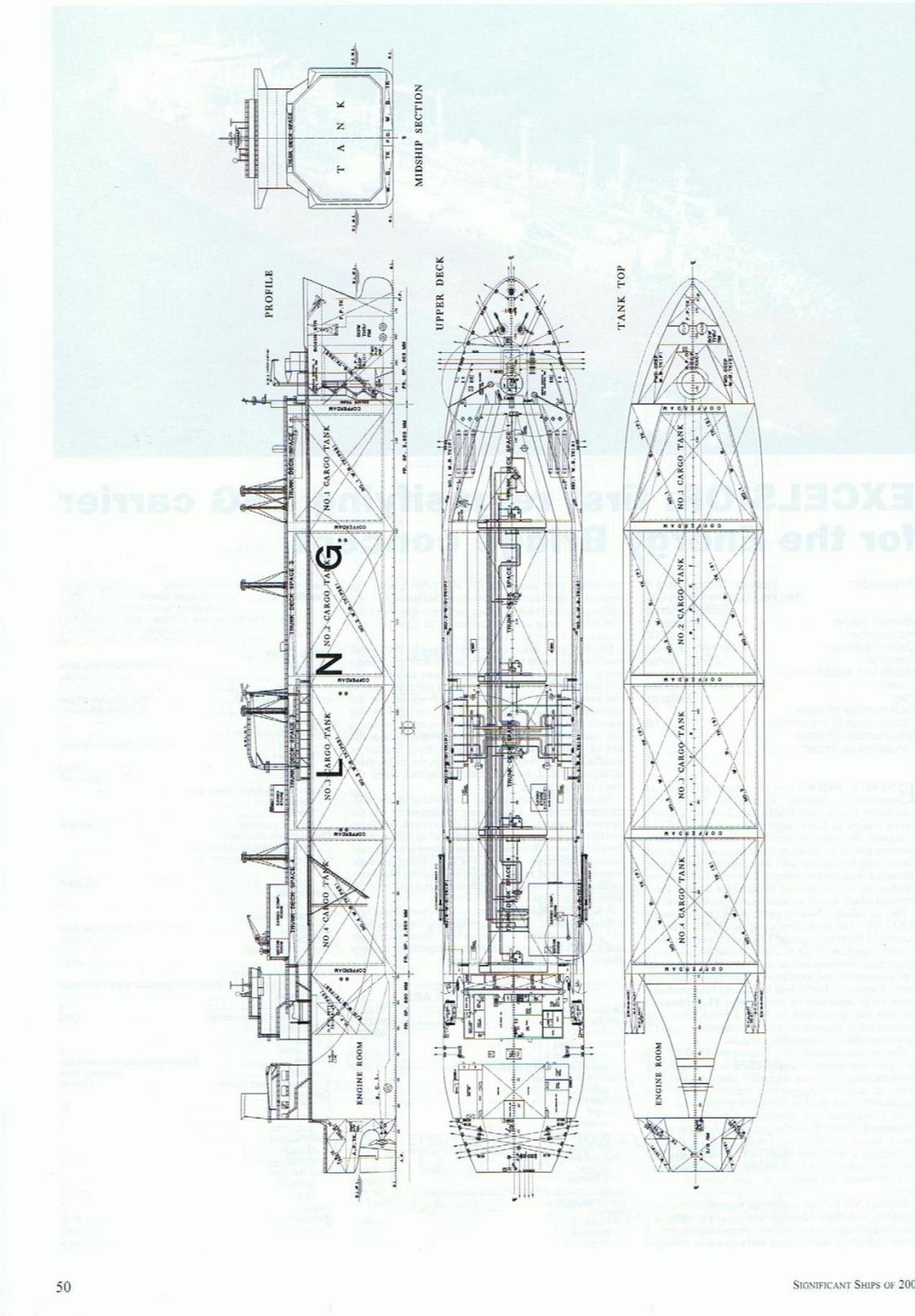
Complement
 Officers 19
 Crew 15
 Suez crew 6

Bow thrusters
 Number 2
 Output, each 1500kW

Stern thruster
 Number 1
 Output 2000kW

Radars 2
 Contract date 13 March 2002
 Launch/float-out date 15 November 2003
 Delivery date 14 January 2005

EXCELSIOR



ETJUHOS YMM3



EXPRESS: LNG re-gasification vessel from Daewoo

Shipbuilder: Daewoo Shipbuilding & Marine Engineering Co., Ltd
 Vessel's name: Express
 Hull No: 2263
 Owner/Operator: EXMAR
 Country: Belgium
 Designer: Daewoo Shipbuilding & Marine Engineering Co., Ltd
 Model test establishment used: SSPA
 Flag: Belgium
 Total number of sister ships already completed (excluding ship presented): 1
 Total number of sister ships still on order: 3

Express, a 74,700dwt LNGRV (liquefied natural gas re-gasification vessel) was delivered by Daewoo Shipbuilding & Marine Engineering Co. Ltd. (DSME) to EXMAR Marine NV of Belgium on May 11, 2009. *Express* is jointly owned by EXMAR and US company Excelerate Energy and is on a 25-year charter to Excelerate Energy. At the time of delivery *Express* was the fourth LNGRV in EXMAR's fleet.

LNGRVs are independent of shore-based re-gasification facilities, being capable of re-gasifying LNG onboard and delivering it directly into the distribution system. *Express* can discharge re-gasified liquid natural gas through a high pressure shore manifold connection or to a subsea pipeline through an internal turret arrangement connected to an offshore mooring buoy. The vessel can also operate as a conventional LNG vessel discharging to a shore-based re-gasification facility.

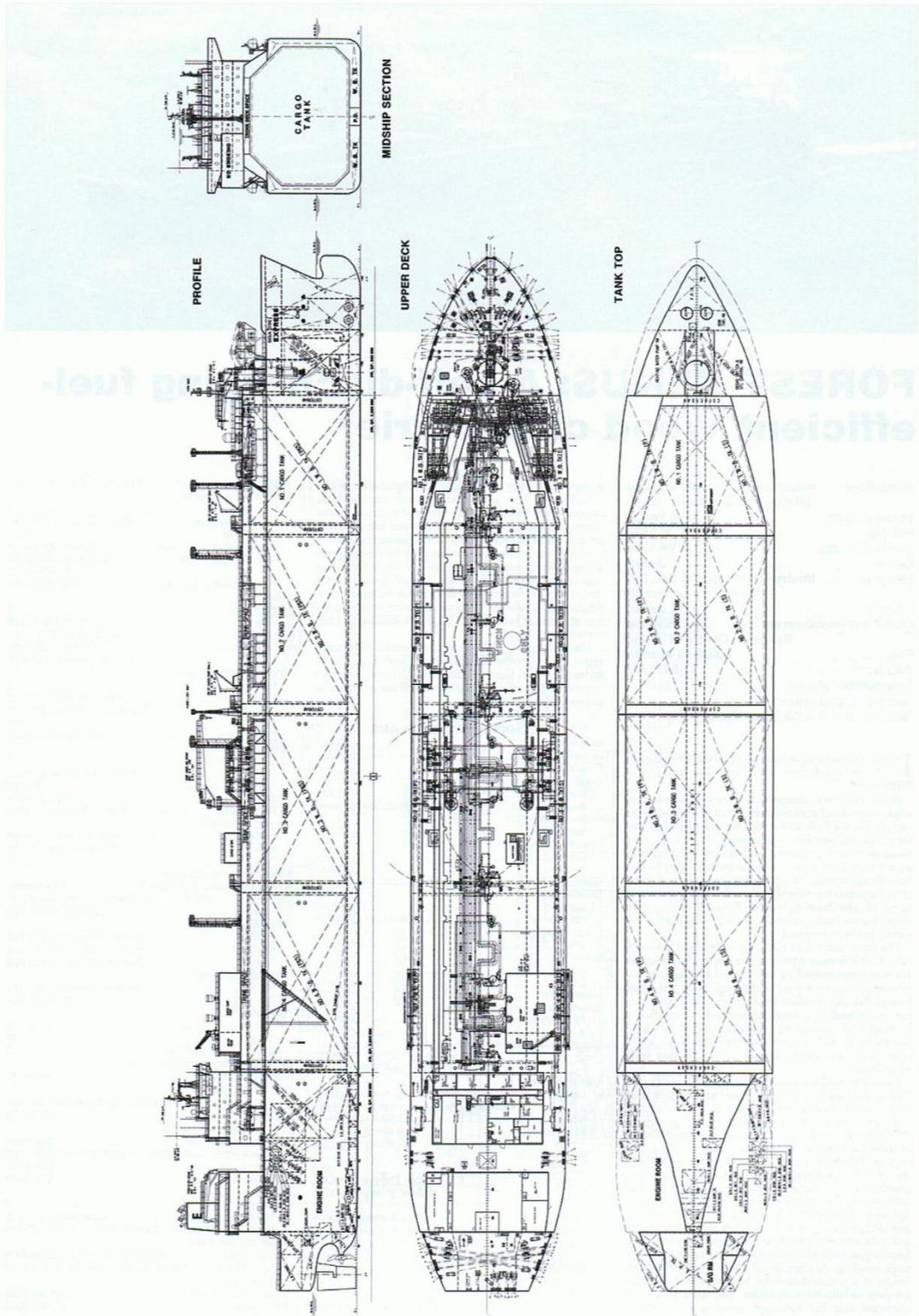
Express has a continuous upper deck with aft sunken deck, a raked stem with bulbous bow and a submerged turret unloading system, a transom stern with open water type stern frame, a semi balanced rudder and a fixed pitch propeller driven by a cross compound type marine steam turbine. The cargo area is of the double-hull type with a double bottom. Cofferdams are located at forward and after part of cargo area and between cargo tanks. Cargo is carried in four centre cargo tanks with the Gaz Transport & Technigaz membrane containment system ("GT NO 96 E-2").

The re-gasification plant, consisting of a number of high pressure pumps, vaporisers, heaters and other equipment is provided in way of No. 1 cargo tank. A SCR (Selective Catalytic NOx Reduction) system is provided for two main boilers and one auxiliary boiler in order to reduce the NOx level.

TECHNICAL PARTICULARS

Length oa: 291.0m
 Length bp: 280.0m
 Breadth moulded: 43.4m
 Depth moulded to main deck: 26.0m
 to upper deck: 32.95m
 Width of double skin side: 2.211m
 bottom: 3.2m
 Draught scantling: 12.4m
 design: 11.6m
 Gross: 100,300gt
 Displacement: 117,300tonnes
 Deadweight: 74,700dwt
 Design: 83,200dwt
 Scantling: 19.2knots
 Speed, service: (90% MCR with 21% sea margin)
 Cargo capacity:
 Liquid volume: 151,000m³
 Bunkers:
 Heavy oil: 5906m³
 Diesel oil: 480m³
 Water ballast: 55,000m³
 Daily fuel consumption:
 Main engine only: 170.3tonnes/day
 Classification society and notations: Bureau Veritas; I +HULL +MACH, Liquefied gas carrier(LNG), Ship Type 2G (membrane tank, 0.25 bar -163C, 500kg/m³), unrestricted navigation, +VeriSTAR Hull, AUT-UMS, +SYS-NEQ-1, SPM/STL, INWATERSURVEY, MON-SHAFT
 % high tensile steel used in construction: 0.2%
 Main engine:
 Design: Cross compound, marine steam turbine
 Model: UA 360
 Manufacturer: KHI
 Number: 1
 Output: MCR: 26,480kW/88rev/min

Gearbox:
 Make: KHI
 Number: 1
 Output speed: 88rev/min
 Propeller:
 Material: Ni-Al-Bronze
 Designer/Manufacturer: Hyundai
 Number: 1
 Fixed/Controllable pitch: Fixed
 Diameter: 8.5m
 Speed (NCR): 85rev/min
 Special adaptations: Class I of ISO 484/1 and class S of ISO 484/1
 Turbine driven alternators:
 Number: 3
 Turbine make/type: MHI/Multi-stage high efficiency turbine AT42CT
 Alternator make/type: HHI/Self-excited, brushless
 Output/speed of each set: 3700kW/1800rev/min
 Diesel driven alternators:
 Number: 1
 Engine make/type: Wartsila 12V32DF / 4-stroke, dual fuel burning
 Type of fuel: MDO/Fuel gas
 Output: 4020kW
 Boilers:
 Number: 2
 Type: Vertical, 2-drum, water tube type
 Make: MHI
 Output, each boiler: 71,000kg/hour x 6.03MPa
 Cargo cranes:
 Number: 2
 Make: TTS Marine Crane AS
 Type: Electro-hydraulically driven
 Performance: 12tonnes (SWL) x 12m/min.
 Other cranes:
 Number: 2
 Make: TTS Marine Crane AS
 Type: Electro-hydraulically driven,
 Task: Engine spare part & provision handling
 Performance: 12tonnes (SWL) x 10m/min.
 Mooring equipment:
 Number: 2 windlasses + 7 mooring winches
 Make: TTS KOCKS GMBH
 Type: Electro-hydraulically driven, high pressure type
 Special lifesaving equipment:
 Number of each and capacity: 2 x 40persons
 Make: UMCOE Schart-Harding
 Type: Totally enclosed type (FRP)
 Cargo tanks:
 Number: 4
 Stainless steel: SUS 316L for cargo system
 Cargo pumps:
 Number: 8
 Type: Cryogenic centrifugal
 Make: Ebara
 Materials: Aluminium alloy casing and impeller
 Capacity (each): 1700m³/h
 Cargo control system:
 Make: Honeywell
 Type: Central computerised system
 Ballast control system:
 Make: Honeywell
 Type: Central computerised system
 Complement:
 Officers: 18
 Crew: 15
 Bow thrusters:
 Make: Brunvoll As
 Number: 2
 Output (each): 1500kW
 Stern thrusters:
 Make: Brunvoll As
 Number: 1
 Output: 2000kW
 Submerged Turret Unloading (STL):
 Make: Advanced Production & Loading AS
 Number: 1
 Capacity: Approx. 500 MMSCFD
 Bridge control system:
 Make: KHI
 Type: UA 360
 Is bridge fitted for one-man operation? Yes
 Fire detection system:
 Make: Consilium
 Type: Addressable
 Fire extinguishing systems:
 Cargo holds: None
 Engine room: High expansion foam system / Kashwa
 Cabins: Portable fire extinguishing system
 Public spaces: Portable fire extinguishing system
 Radar:
 Number: X-band(one set) & S-band(one set)
 Make: SAM Electronics
 Model(s): Chart radar 1100
 Integrated bridge system:
 Make: SAM Electronics
 Model: Chart plot 1100
 Waste disposal plant:
 Incinerator: Kangrim KEI-70SDA
 Sewage plant: Jonghap AEROB-18
 Contract date: 10 January 2006
 Launch/float-out date: 21 June 2008
 Delivery date: 11 May 2009





FERNANDO TAPIAS: Daewoo-built LNG tanker for Spanish owner

Shipbuilder: Daewoo Shipbuilding & Marine Engineering Co Ltd, Korea
 Vessel's name: Fernando Tapias
 Hull number: 2205
 Owner/operator: Naviera F Tapias Gas SA, Spain
 Designer: Daewoo Shipbuilding & Marine Engineering Co Ltd, Korea
 Flag: Spain
 Total number of sister ships already completed: Nil
 Total number of sister ships still on order: 1

FERNANDO TAPIAS has been built for the transportation of liquefied natural gas (LNG), and special attention has been paid in her design to the facilities at loading and discharging berths worldwide, to ensure compatibility of mooring arrangements, fender contact areas, gangway and manifold positions, and other aspects. Laid out with a continuous single deck, and a sunken aft deck, the vessel has four cargo tanks, constructed on the Gaz Transport membrane system (GT No 96 E-2), positioned in a double-hull configuration which is extended above the deck to form a trunk.

Gas is maintained at a temperature of -163°C with a maximum boil-off rate of less than 0.15% fully loaded cargo volume. Primary/secondary barriers of 36% nickel-steel (Invar) alloy are fitted in the cargo tanks, with plywood boxes filled with expanded perlite forming primary/secondary insulation. Underdeck passageways in the trunk deck space provide fore and aft access, and a duct keel in the double bottom serves as a pipe and cable passage.

The cargo handling systems are designed to load/discharge cargo within 12 hours, using two sets of 1700m³/h pumps and one stripping/spray pump in each tank, forming a complete assembly within a 'tripod mast' construction with Saab radar beam-type level gauges, and all fittings and pipes. Vapour handling equipment such as two high-duty compressors, two low-duty compressors, one main and one forcing vaporiser, and two boil-off/warm-up heaters, are arranged in the cargo machinery room.

The main propulsion unit is a Kawasaki UA-360 cross-compound steam turbine, developing 36,000shp at 88rev/min (behind the gearbox). The unit has high- and low-pressure turbines, double-

reduction gearing, main condenser, and astern turbine. Two dual-fuel boilers supply steam for the main turbine, steam auxiliaries, and turbo-generators. Two of the latter are installed for electrical power together with one diesel-powered set. Each develops a similar output of 3450kW. Current is transmitted to three switchboards (main, cargo, and emergency) located in separate rooms. An integrated automation system is fitted, and control and monitoring is carried out from the cargo and engine control rooms.

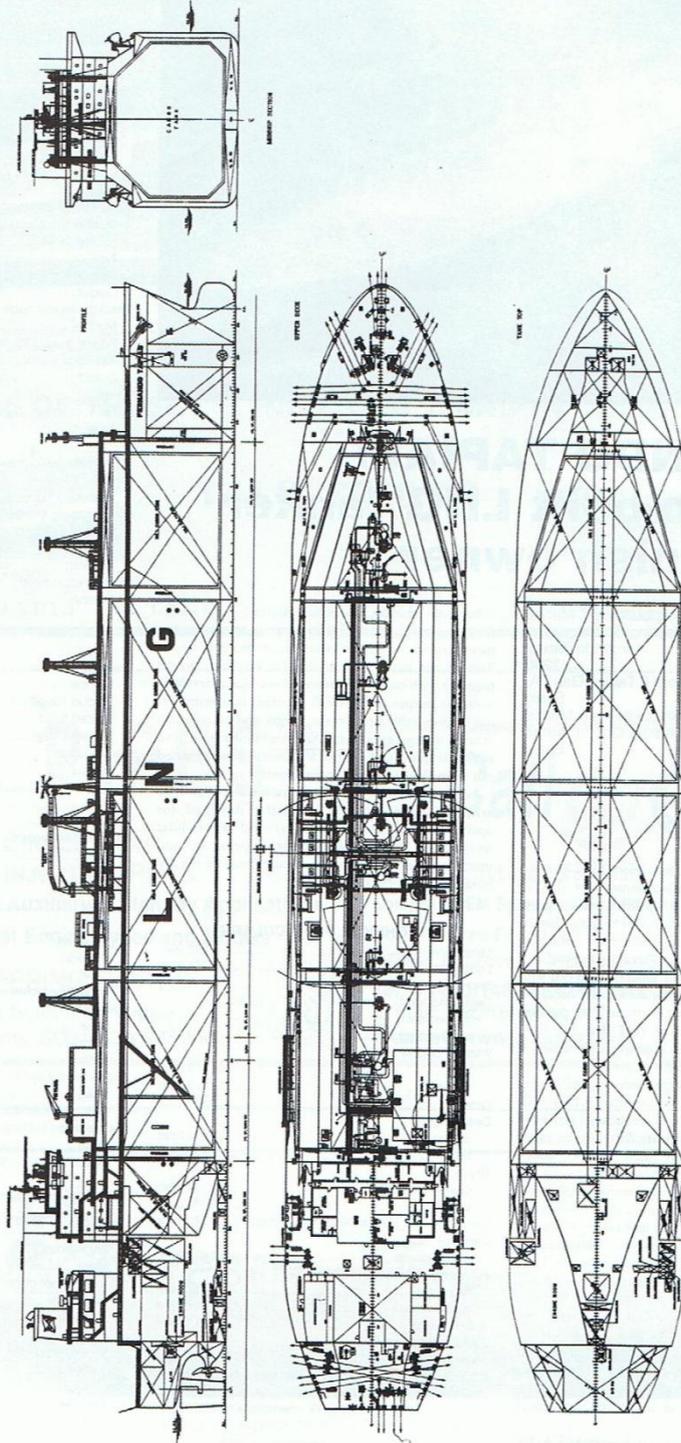
Accommodation and navigation spaces are arranged right aft, with the latter designed for optimum operational safety around a modular workstation, fitted for one-man operation, and meeting all design and layout requirements of the BV notation +SYS-NEQ-1.

TECHNICAL PARTICULARS

Length, oa	298.00m
Length, bp	268.80m
Breadth, moulded	43.40m
Depth, moulded	
to main deck	26.00m
to trunk deck	32.75m
Width of double skin	
side	2.21m
bottom	3.20m
Gross	94,822gt
Deadweight	
design	72,367dwt
scantling	79,364dwt
Draught	
design	11.42m
scantling	12.12m
Speed, service (90% MCR: 21% sea margin)	19.50 knots
Cargo capacity	
liquid volume	140,627m ³
Bunkers	
heavy fuel	6,004m ³
diesel oil	502m ³
Water ballast	53,108m ³
Fuel consumption	
main engine only	165.60tonnes/day
Classification	Bureau Veritas, I + Hull, + MACH, Liquefied Natural Gas Carrier, Ship Type 2G, (membrane tank, 0.25bar, -163°C, 500kg/m ³), unrestricted navigation, + VeriSTAR-HULL, AUT-IMS, AUT-PORT, +SYS-NEQ-1, In Water Survey, MON-SHAFT
Percentage of high-tensile steel used in construction	Nil

Steam turbine	
Design	Cross-compound impulse turbine
Manufacturer	Kawasaki Heavy Industries
Model	UA-360
Number	1
Output	MCR: 36,000shp/88rev/min NCR: 32,400shp/85rev/min
Propeller	
Material	Cunial
Manufacturer	Lips
Number	1
Pitch	Fixed
Diameter	8500mm
Speed	88rev/min (MCR)
Steam-turbine driven alternators	
Number	2
Turbine make	Mitsubishi Heavy Industries
Type	Multi-stage
Alternator make	Hyundai Heavy Industries
Output	2 x 3450kW/1800rev/min
Diesel-driven alternator	
Number	1
Engine make	Ssangyong Heavy Industries
Alternator make	Hyundai Heavy Industries
Output	1 x 3450kW/720rev/min
Boilers	
Number	2 plus 1 low-pressure steam generator
Type	2 x vertical two-drum 1 x horizontal tubular
Makers	Mitsubishi Heavy Industries and Donghwa Entec
Output	2 x 56tonnes/h; 1 x 6.5tonnes/h
Hose-handling cranes	
Number	2
Make/type	Hydralift/electro-hydraulic
Capacity	2 x 12tonnes
Mooring equipment	
Number	2 x mooring winch/windlass 7 x mooring winch
Make	Kocks
Type	High-pressure hydraulic
Cargo tanks	
Number	4
Product range	LNG
Coated tanks	No
Stainless steel	No
Cargo pumps	
Number	8
Type	Submerged electrical
Make	Ebara International
Capacity	8 x 1700m ³ /h
Cargo control system	
Type	Integrated automation system
Makers	Honeywell Korea
Ballast pumps	
Make	Shinko
Type	Electric vertical centrifugal
Complement	
Officers	21
Crew	16
Repair/Suez crew	6
Bow thruster	
Make	Brunvoll
Number	1
Output	1 x 1600kW
Bridge control system	
Make	STN Atlas
One man operation	Yes
Fire detection systems	
Make	Consilium
Type	25 heat detectors; 6 flame detectors; 235 smoke detectors
Fire extinguishing systems	
Cargo spaces	Dry powder, water spray, nitrogen
Make	NK Fire Protection
Engine room	High-expansion foam
Make	Kashiwa
Waste disposal plant	
Incinerator	
Make	Hyundai-Atlas
Model	Maxi T150 SL W/S
Waste compactor	
Make	Metos Marine
Model	Uson UP-10
Sewage plant	
Make	Jong-Hap
Model	AEROB-18
Contract date	31 March 2000
Launch/float-out date	3 November 2001
Delivery date	30 September 2002

FERNANDO TAPIAS



FRISIA BOM



GDF Suez Point Fortin: 154,900m³ type LNG carrier from Japan

Shipbuilder:..... **Koyo Dockyard co., Ltd. Of Imabari Group**
Vessels name:..... **GDF Suez Point Fortin**
Hull No:..... **2263**
Owner/operator:..... **Los Halillos Shipping co., SA Panama**
Country:..... **Panama**
Model test establishment used:..... **Shipbuilding research centre of Japan**
Flag:..... **Panama**
IMO number:..... **9375721**
Total number of sister ships already completed (excluding ships presented):..... **2**
Total number of sister ships still on order:..... **0**

IMABARI has opened up further avenues for the group to expand into with the delivery of *GDF Suez Point Fortin*. The vessel was delivered to its owner GDF Suez on 16 February. The vessel is owned by a consortium led by Mitsui OSK Lines and will be operated by Los Halillos Shipping.

GDF Suez Point Fortin's main feature is that its No 1 tank is of a horizontally trapezoid shape, making it the first of its kind, in order to use maximum tank capacity despite the compact hull to ensure longitudinal hull structure. It is one of only three vessels with this type of tank capacity.

The hull structure of the vessel was designed and developed under Lloyd's Register's (LR) notation ShipRight (SDA, FDAplus, CM). SDA and FDAplus analysis were carried out in close cooperation with LR London. *GDF Suez Point Fortin* has been designed with a fatigue life set at 40 years.

Reinforced Polyurethane foam (R-PUF) has been used as thermal insulation for the cargo tanks and cargo piping. Formerly, Hydro-Chloro-Fluoro-Carbon (HCFC) was employed as a gas in micro bubbles of R-PUF. In comparison the HCFC, ODP and GWP has less CO₂ than the old method. Imabari has used a new material onboard *GDF Suez Point Fortin* that has been developed from a Japanese manufacturer that still keeps the same thermal conductivity as the previous material.

GDF Suez Point Fortin is 289.93m in length overall, 44.70m wide and has a 26m depth with a design draught of 11.73m and a deadweight of 72,354dwt. It is powered by a Kawasaki UA - 400 type cross compound impulse steam turbine with double reduction gear that can run on either heavy fuel oil (HFO) or liquefied natural gas (LNG) and is capable of 19.5knots at 80.4MCR.

TECHNICAL PARTICULARS

Length oa:..... 289.93m
Length bp:..... 276.00m
Breadth moulded:..... 44.70m
Depth moulded:..... 26.00m
To main deck:..... 26.00m
To upper deck:..... 26.00m
To other decks:..... 33.12m (trunk deck)
Width of double skin:..... 2.51m
Side:..... 2.51m

Bottom:..... 3.20m
Draught:..... 12.60m
Scantling:..... 11.73m
Design:..... 101.129gt
Gross:..... 72,354dwt
Deadweight:..... 85,547dwt
Design:..... 19.5knots (80.4%MCR output)
Speed, service:..... 154,913m³
Cargo capacity:..... 6460m³
Liquid volume:..... 700m³
Heavy oil:..... 53,690m³
Diesel oil:..... 163.4tonnes/day
Water ballast:..... LR +100A1, Liquefied Gas Tanker, Ship Type ZG, Methane(LNG) in membrane tanks, Maximum vapour pressure 0.25bar, Minimum temperature -163°C, ShipRight(SDA,FDA plus, CM), *IWS, L1, +LMC, UMS, NAV1, IBS, ICC

Main engines
Design:..... Kawasaki Heavy Industries Ltd.
Model:..... Kawasaki UA - 400 type cross compound impulse steam turbine with double reduction gear
Manufacturer:..... Kawasaki Heavy Industries Ltd.
Number:..... 1 set
Type of fuel:..... HFO and/or LNG
Output of each engine:..... MCR 29,420kW x 81rpm
NCR 26,480kW x 78.2rpm

Gearboxes
Make:..... Kawasaki Heavy Industries Ltd.
(Reduction gear is included in main turbine set.)
Model:..... UA420/80 - S (tandem articulated, double reduction gear)

Propeller
Material:..... Ni-Al-Bronze
Designer/manufacturer:..... Mitsubishi Heavy Industries Ltd.
Number:..... 1 set
Fixed/Controllable pitch:..... Fixed type

Diesel-driven alternators
Number:..... 1 set
Engine make/type:..... Yanmar co., Ltd / 4 - cycle diesel engine
Type of fuel:..... Diesel oil or Marine gas oil
Output/speed of each set:..... 3604kW/720rpm
Alternator make/type:..... Nishishiba electric co., Ltd/ Totally enclosed, brushless

Output/speed of each set:..... 3250kW/720rpm
Turbine make/type:..... Steam turbine-driven alternators stem driven, multi stage condensing
Output/speed of each set:..... 3250kW/8145kW
Alternator make/type:..... Nishishiba electric co. Ltd/ Totally enclosed brushless

Output/speed of each set:..... 3250kW x 1800rpm
Boilers
Number:..... 2 sets
Type:..... Kawasaki UME 66/53

Make:..... Kawasaki Heavy Industries Ltd
Output each boiler:..... Max evaporation 66,000kg/h
Other cranes
Number:..... 2 sets

Make:..... Sekigahara Seisakusho Ltd
Type:..... Electro-hydraulic high-pressure
Tasks:..... Hose handling
Performance:..... Hoisting load 22m/ working radius 22m - 4.6m

Mooring equipment
Number:..... Windlass 2 sets/ Mooring winch 8 sets
Make:..... Fukushima Ltd
Type:..... Electro-hydraulic Low-pressure
Special lifesaving equipment
Number of each and capacity:..... 2 sets x 50 persons
Make:..... Ernst Hatecke
Type:..... Enclosed

Cargo tanks
Number:..... 4 tanks (membrane type)
Grades of cargo carried:..... Liquefied natural gas
Product range:..... Max specific gravity 0.5 at -163°C
Stainless steel - structure/piping:..... Stainless steel (304L)

Cargo pumps
Number:..... 8 sets
Type:..... Vertical submerged
Make:..... Shinko Industries Ltd
Stainless steel:..... Ball bearing
Capacity:..... 1700m³ x 160m

Cargo control system
Make:..... Yokogawa Electric Corp.
Type:..... Integrated automation system

Ballast control system
Make:..... Yokogawa Electric Corp.
Type:..... Integrated automation system

Complement
Officers:..... 13
Crew:..... 16
Suez/Repair crew:..... 6

Bow thrusters
Make:..... Kawasaki Heavy Industries Ltd
Number:..... 1 set
Output:..... 2200kW

Bridge control system
Make:..... Japan Radio co., Ltd.
Type:..... Integrated navigation system
One-man operation:..... Yes

Fire detection system
Make:..... Nippon Hakuyo
Type:..... FF - 1515 - 4

Fire extinguishing system
On deck:..... Dry chemical powder fire extinguishing system
Make/Type:..... Unitor
Engine room:..... High expansion foam fire extinguishing system

Make/Type:..... Kashiwa-teck
Cabin:..... Seawater
Public spaces:..... Seawater

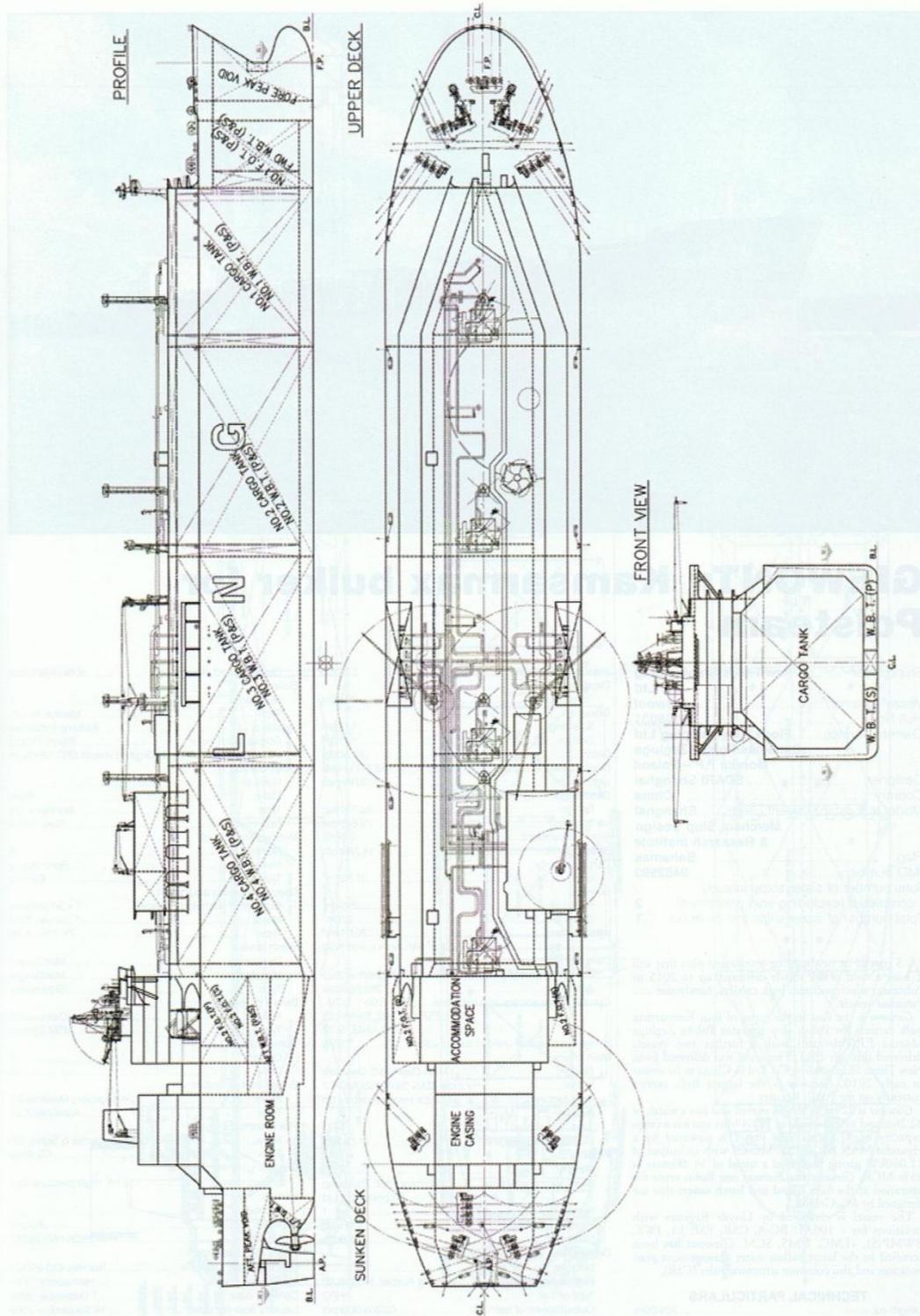
Radars
Number:..... 3 sets (X-Band/2 S-Band/1)
Make:..... Japan Radio Co., Ltd
Model:..... JMA - 9122 - 9XA,
NKE - 1125 - 9, JMA - 9132 - SA

Waste disposal plant
Incinerator:..... Sunflame co., Ltd
Model:..... OSV-600SDAI

Waste compactor:..... Electrolux professional AB
Model:..... 41 80 10 (TT100)
Sewage plant:..... Taiko Kikai Industries co., Ltd

Contract date:..... 21 November 2005
Launch/float-out date:..... 12 August 2008
Delivery date:..... 16 February 2010

GDF SUEZ POINT FORTIN





HANJIN MUSCAT: satisfying Korea's fuel requirements

Shipbuilder:Hanjin Heavy Industries Co Ltd, Korea
 Vessel's name:Hanjin Muscat
 Hull number:N-054
 Owner/operator:Hanjin Shipping Co Ltd, Korea
 Designer:Hanjin Heavy Industries Co Ltd, Korea
 Flag:Panama
 Total number of sister ships already completed:
 Total number of sister ships still on order:2

SUCH is the demand for liquefied natural gas (LNG) to satisfy the domestic demands of the Korean Gas Corp (KOGAS), that three out of the four major Korean shipbuilders who are today serious players in the world market for this type of ship, are currently involved with an extensive KOGAS newbuilding programme which will run for a number of years yet. Present contracts call for vessels of around 138,000m³ capacity, suitable for operation between Gulf ports and Korean terminals, but, as the three reports included in this review show, within these parameters, each builder/owner combination has left its own mark.

Hanjin Muscat is a larger version of Hanjin Pyeong Taek (Significant Ships of 1995), and uses the same Gaz Transport No 96-2 membrane cargo containment system, featuring a four-tank format with the tanks contained in a complete double-hull structure which includes ship's sides and bottom, transverse bulkheads, and upper deck trunk. The side and bottom spaces are sloped at top and bottom, and are divided by the duct keel to form P&S integral ballast tanks. This double structure not only protects the tanks from external damage, but insulates the outer hull against critical steelwork fractures caused by the low temperature (-163°C) and atmospheric pressure at which cargoes are carried. A considerable amount of structural analytical work was carried out for these new larger membrane designs by the Korean Register of Shipping.

Tank insulation is formed by primary and secondary membranes of 0.70mm Invar sheets (a product containing 36% nickel steel) in conjunction with expanded Perlite beads contained in plywood boxes, which are attached to the inner hull by stud bolts. This combination is able to sustain the liquid pressure and static and dynamic loads, and to limit the daily boil-off rate to 0.15% of cargo volume. A tripod mast is built within each tank, to which the filling line and two Ebara 1700m³/h electric, submersible pumps are attached. These are used for unloading purposes only, loading being carried out by shore pumps, with vapour produced in the operation returned to shore by the ship's two 32,000m³/h compressors.

The performances of the equipment mentioned are all substantially higher than those fitted on Hanjin Pyeong Taek, reflecting the increased capacity of the newer vessel. This continues with other items supplied, such as a 26,000kg/h main vaporiser and 7600kg/h forcing vaporiser, 13,800Nm³/h inert-gas generator, two 140Nm³/h nitrogen generators, and two 1250m³/h vacuum pumps. Four 50m³/h stripping/spray pumps, a 550m³/h emergency cargo pump and two sets of 20,000kg/h boil-off/warm-up heaters are also fitted.

Two personnel can operate and monitor the entire ship from a centralised administration and control centre on accommodation deck D, using two separate Yamatake-Honeywell TDC 3000 Basic automation systems. These serve cargo/ballast operations and machinery/electric generation, respectively, with Whessoe tank level gauges, a Foxboro custody transfer system, and a Mitsubishi total boil-off gas control system. Mitsubishi also supplied a loading calculator to assist cargo operations, together with an auto combustion control, burner management and main turbine controls. Other equipment includes an AMCO turbo feed pump control system and Kvaerner ship performance monitors for the machinery installation.

A Mitsubishi MS 40-2 cross-compound steam turbine developing 38,900shp drives a FP propeller through a double-reduction gearbox for a service speed of 20.3knots, using steam generated from two vertical, two drum watertube boilers, burning oil or boil-off gas, or a combination of both. Two 3450kW turbo-alternators and a similar sized diesel-alternator set satisfy electrical requirements. A water scoop system is provided for cooling the main condenser.

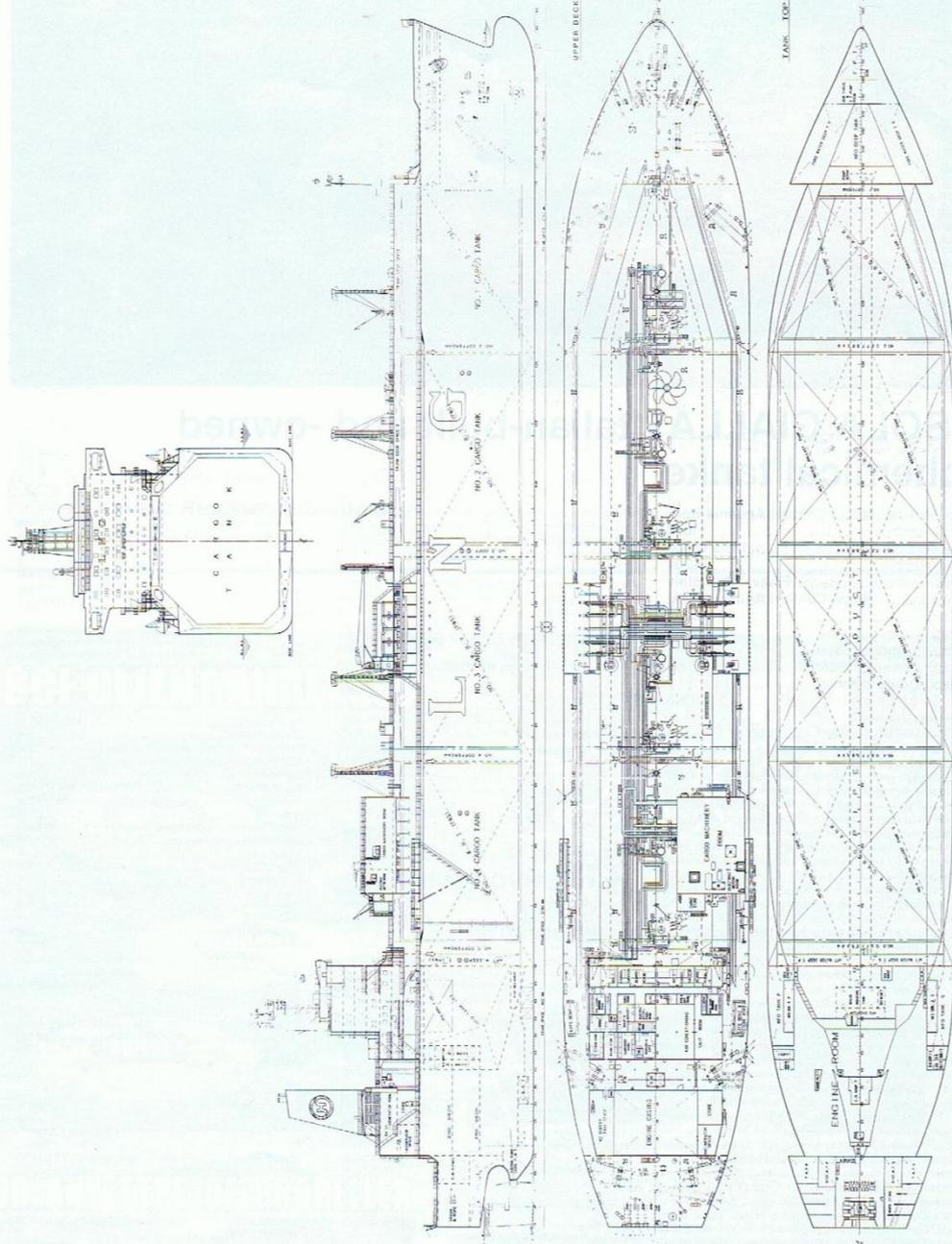
Mitsubishi also supplied one of its Total Navigation Systems, which is integrated with three radars, echosounder, doppler sonar and docking system supplied by Atlas Elektronik. Additional aids include a Tokimec chartplotter and two GPS navigators.

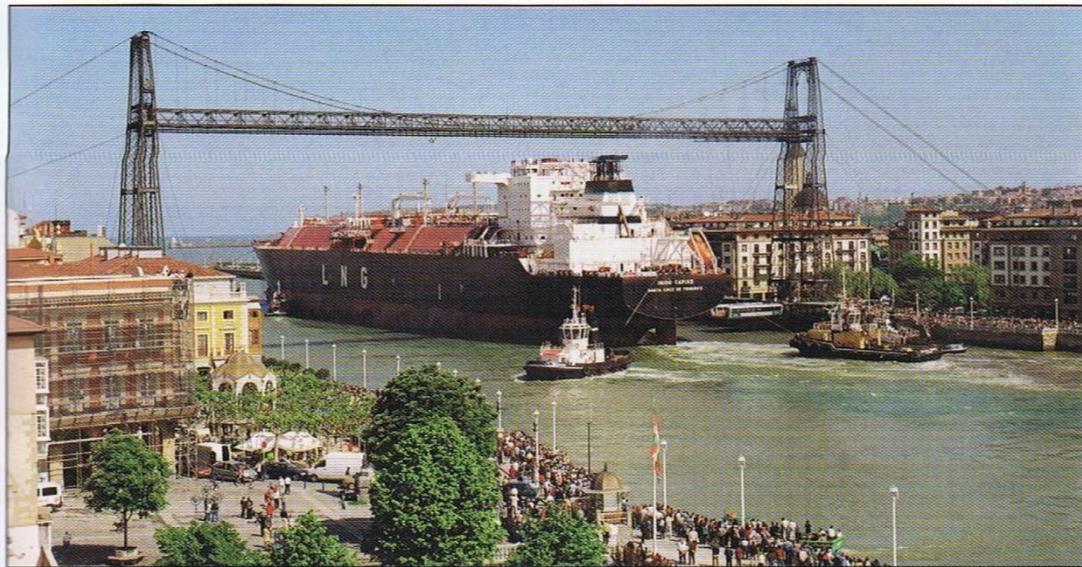
PRINCIPAL PARTICULARS

Length, oa	280.00m
Length, bp	268.50m
Breadth, moulded	43.00m
Depth, moulded	
to main deck	26.20m
to trunk deck	32.55m
Width of double skin	
side	2.20m
bottom	3.00m
Gross	93,765gt
Deadweight	
design	68,524dwt
scantling	75,463dwt
Draught	
design	11.30m
scantling	12.00m
Speed, service with 21% sea margin	20.30knots
Cargo capacity	
liquid volume	138,366m ³

Bunkers	
heavy oil	6046m ³
diesel oil	235m ³
Water ballast	52,488m ³
Fuel consumption	
main engine only	201tonnes/day
Classification	Korean Register of Shipping +KRS1-Liquefied Gas Carrier, +KRM1-UJA, 2Q3M(R)0.25bar, -163°C, 0.53G(LGC), (LWS) also Bureau Veritas +1/3E, Liquefied Gas Carrier/LNG, Deep Sea, AUT-MS*
Percentage of high-tensile steel used in construction	Nil
Main engine	
Design	Mitsubishi Heavy Industries Ltd
Model	MS 40-2 steam turbine
Manufacturer	Mitsubishi Heavy Industries Ltd
Number	1
Output	38,900shp/83rev/min
Gearbox	
Make	Mitsubishi Heavy Industries Ltd
Type	Double-helical dual-tandem articulated
Number	1
Propeller	
Material	Nickel-aluminium-bronze
Manufacturer	Hyundai Heavy Industries Ltd
Number	1
Pitch	Fixed
Diameter	8500mm
Speed	83rev/min
Steam turbine-driven alternators	
Number	2
Turbine make	Mitsubishi
Alternator make/type	Hyundai/HFJS 714-44E
Output	2 x 3450kW/1800rev/min
Diesel-driven alternator	
Number	1
Engine make	Hyundai/Wärtsilä
Alternator make	Hyundai
Output	3450kW/720rev/min
Boilers	
Number	2
Type	Two drum (steam and water) water tube, dual fuel
Make	Mitsubishi
Output	2 x 68,000kg/h(max)/59,000kg/h(normal)
Hose-handling cranes	
Number	2
Make/type	Dong Nam/electro-hydraulic
Capacity	2 x 10tonnes/22m
Mooring equipment	
Number	2 x windlass; 9 x mooring winch
Make	Brissonneau et Lotz(BLM)
Type	Electro-hydraulic
Cargo/ballast control systems	
Make	Mitsubishi
Type	MCS-6100A
Complement	
Officers	24
Crew	15
Travelling workers	8
Cargo tanks	
Number	4
Product range	Liquefied natural gas
Coated tanks	Gaz Transport cargo containment system with Invar membrane
Cargo pumps	
Number	8 plus 4 stripping
Type	12EC-24 submerged centrifugal
Make	Ebara
Capacity	8 x 1700m ³ /h
Bow thruster	
Make	Nakashima/TC-280tonne
Number	1
Fire detection system	
Make	Consilium Marine
Type	CS 300
Fire extinguishing systems	
Cargo area	Dry powder
Make	Fain
Engine room	Fixed high-pressure CO ₂
Radars	
Number	3 (2 x S-band; 1 x X-band)
Make	STN Atlas
Models	Atlas 9600
Satellite navigation system	
Make	JRC
Model	JLR-6800 DGPS
Computers on ship	
Number	8
Make	Mitsubishi
Waste disposal plant	
Incinerator	
Make	Kangrim
Model	KIN-50 SOA
Waste compactor	
Make	Metos
Model	UP-10
Sewage plant	
Make	Evac
Model	AHM 0122
Contract date	24 December 1996
Launch/float-out date	30 April 1998
Delivery date	30 July 1999

HANJIN MUSCAT





INIGO TAPIAS: satisfying Spain's increasing LNG requirements

Shipbuilder:.....IZAR (Astillero Sestao, Bilbao), Spain
 Vessel's name:.....*Inigo Tapias*
 Hull number:.....319
 Owner/operator:.....Naviera F Tapias SA, Spain
 Designer:.....IZAR
 Model test establishment used:.....MARIN, The Netherlands
 Flag:.....Spain
 Total number of sister ships already completed:.....Nil
 Total number of sister ships still on order:.....4 (contract shared with IZAR (Puerto Real))

A PROJECTED 50% increase in Spain's consumption of gas has initiated this contract, for vessels equalling in capacity the largest yet built, which re-introduces construction of LNG tankers into the country's shipyards after a lapse of more than 30 years. Although designed to load/unload at all the world's current terminals, *Inigo Tapias* will normally be employed transporting gas from Trinidad and Tobago to Spain, with hull form, propulsion and power systems, developed for maximum energy economy on what is virtually a liner service. To this end, Schneckluth wake-equalising ducts have been fitted at the stern, in front of a five-bladed FP propeller, in an arrangement claimed to reduce power requirements by 1.50%.

The proven reliability of steam turbine propulsion, along with the ability of that system to burn boil-off gases in the boilers, is demonstrated by the fitting of a conventional (for this type of vessel) machinery installation centred upon a Kawasaki package, comprising a main propulsion turbine developing 28,000kW at 83rev/min, two 3150kW turbo-generators, main feed pump turbines, and reversible double-reduction gearing, all assembled at the shipbuilder's Ferrol works. A 3150kW diesel-alternator set is installed and an 1800kW electric bow thruster is fitted. The two Mitsubishi boilers each have an output of 65,000kg/h and are arranged to burn heavy oil, boil-off gas, or a combination of both.

Inigo Tapias is a single-deck vessel with sunken aft deck, and all accommodation and navigating spaces aft, built with principal dimensions which differ slightly from those of other, similar sized vessels (see *Significant*

Ships of 2002), resulting in a slightly longer, narrower hull form. This is in order to meet a beam restriction on the building berth at the Sestao yard. The machinery casings and accommodation are not integrated, in order to minimise vibration transmission, and the design satisfies the requirements of a Type 2G tanker suitable for the carriage of liquid natural gas of SG 0.46 at -163°C. Maximum boil off rate is 0.15% cargo volume.

The four cargo tanks, which extend above the deck to form a trunk, are built within a complete double-hull structure with integral spaces utilised as water ballast tanks, in accordance with a Gaz Transport/Technigas NO96-L2 membrane technique, using Invar stainless steel sheet with a 36% nickel content for the primary and secondary barriers. Between these, and the secondary barrier/shell, perlite granules in plywood boxes are inserted.

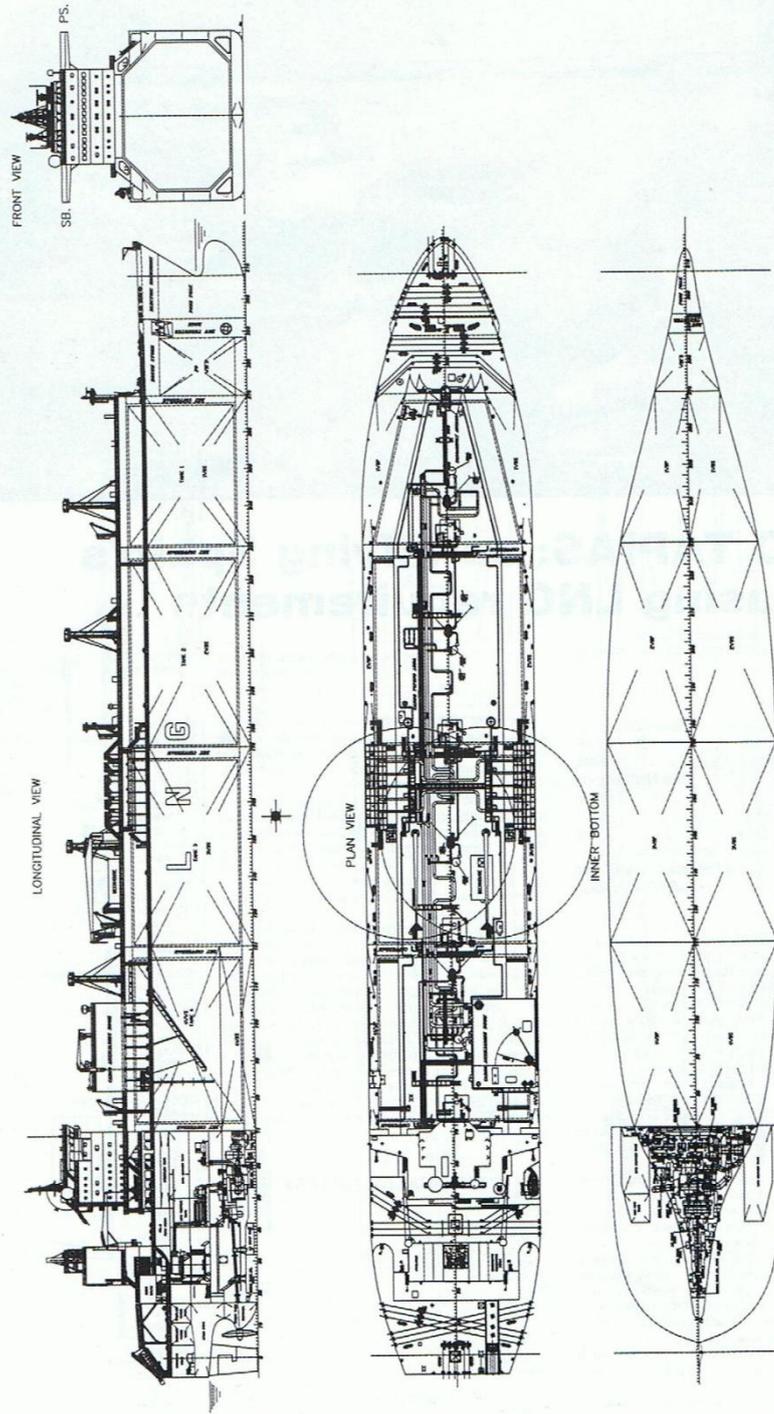
The cargo handling systems can discharge the vessel in 12 hours using two 1700m³/h electric submerged pumps, and one 50m³/h stripping pump, in each tank, supplemented by a 530m³/h emergency cargo pump. Each tank has a liquid manifold; vapour manifold; stripping manifold and cooling manifold, with the liquid pipelines running to the bottom of the tanks and the vapour line connected at the top. Included in the cargo systems are 2 x 30,000m³/h high-duty, and 2 x 8000m³/h low-duty, compressors; two 23,000kg/h main heaters and 1 x 20,000kg/h LNG vaporiser. The forcing vaporiser capacity is 6950kg/h; the inert gas generator is rated at 15,000Nm³/h and the two nitrogen generators each produce 120Nm³/h.

TECHNICAL PARTICULARS

Length, oa	284.40m
Length, bp	271.00m
Breadth, moulded	42.50m
Depth, moulded	-
to main deck	25.40m
to trunk deck	32.20m
Width of double skin	-
Gross	93,450gt
Draught	-
design	11.40m
scantling	12.30m
Deadweight	-
design	68,200dwt
Speed	-
service	19.50knots
ballast trial, at 90% MCR	21.00knots
Cargo capacity	-
liquid volume (100% full)	138,000m ³
liquid volume (98.5% full)	135,930m ³
Bunker capacity	-

Water ballast	-
Classification	Lloyd's Register of Shipping, +100A1, Liquefied Gas Tanker, Ship Type 2G, Methane in Membrane Tanks, Max. Pressure 0.25bar, Min Temperature -163°C, +LMC, UMS, POFIT, SDA, IWS, SCM, LI, FDA, NAV1, IBS, ES, TCM, CCS
Main engine	-
Steam turbine	-
Design	Cross-compound impulse
Manufacturer	Kawasaki Heavy Industries
Model	-
Number	1
Output	28,000kW/83rev/min
Gearbox	-
Make	Kawasaki
Type	Double-reduction
Propeller	-
Manufacturer	Navalpis
Number of blades	5
Number	1
Pitch	Fixed
Diameter	8700mm
Speed	83rev/min
Steam-turbine-driven alternators	-
Number	2
Output	2 x 3150kW
Diesel-driven alternator	-
Number	1
Output	1 x 3150kW
Boilers	-
Number	2 x water tube, dual fuel
Make	Mitsubishi Heavy Industries
Output	2 x 65,000kg/h
Hose-handling cranes	-
Number	2
Duty	2 x 12tonnes swl
Cargo tanks	-
Number	4 x membrane type
Design	Gaz Transport/Technigas
Type	NO96-L2
Product range	LNG
Coated tanks	No
Stainless steel	No
Cargo pumps	-
Number	8
Type	Electric submerged
Make	-
Capacity	8 x 1700m ³ /h
	4 x 450m ³ /h, stripping
Ballast pumps	-
Make	-
Capacity	3 x 2500m ³ /h; 1 x 350m ³ /h ejector; 1 x 200m ³ /h ejector
Complement	-
Stern appendage	Schneckluth wake-equalising ducts
Bow thruster	-
Make	-
Number	1
Output	1 x 1800kW
Contract date	-
Launch/float-out date	-
Delivery date	1 August 2003

INIGO TAPIAS



MAERSK KOWLOON



MAERSK QATAR: 145,600m³ LNG carrier for RasGas project

Shipbuilder:..... Samsung Heavy Industries Co Ltd, Korea
 Vessel's name:..... *Maersk Qatar*
 Hull number:..... 1562
 IMO number:..... 9321732
 Owner/operator:..... AP Möller-Maersk Group, Denmark
 Designer:..... Samsung Heavy Industries Co Ltd, Korea
 Model test establishment used:..... Samsung Ship Model Basin, Korea
 Flag:..... Danish International Shipping Register
 Total number of sister ships already completed:..... 11 (different owners)
 Total number of sister ships still on order:..... 7

THE diversity of the Möller-Maersk Group is difficult to measure, but some idea of its extent is demonstrated in this edition of *Significant Ships* where four of this leading owner's newbuildings are featured, including the largest container ship in the world, together with this vessel - one of the largest LNG tankers in service, alongside two 'baby-size' box ships. Equally, Samsung can point to its own varied output, and a rise to becoming a world leader in LNG carrier design in just seven years since delivering the first ship of this type.

Maersk Qatar is a development of Samsung's standard design, which conforms closely to what has become an industry 'norm', offering around 140,000m³ capacity. In fact, *Maersk Qatar*, with some slight 'tweaking' of length and beam over earlier ships, will load nearly 6000m³ more than that, in its operations on the RasGas project. The design features a double-skin hull with side spaces joined with top and bottom wing tanks arranged to carry water ballast. These enclose four individual cargo tanks, separated by cofferdams, and constructed in accordance with the Gaz Transport and Technigas (GTT) Mk 3 containment system for the carriage of LNG cargoes at cryogenic temperatures (-163°C).

These tanks extend above the upper deck and are enclosed in a trunk which also provides access passages forward and aft. The containment system, which is designed to limit the daily boil-off rate to 0.15% cargo volume, is complemented by three Ebara 1700m³/h electric submersible pumps, capable of discharging cargo in 12 hours, following pre-cooling by LNG spray.

Despite the fact that it does hold contracts for both low-speed diesel and diesel-electric-powered LNG tankers, Samsung has retained the 'traditional' steam turbine propulsion system for *Maersk Qatar*. This makes

use of a Kawasaki UA400, cross-compound, direct-reversible, impulse-type unit developing 29,050kW and driving an FP propeller at 90rev/min for a service speed of 20.6knots. A double-reduction, articulated gearbox is integrated with the main turbine. Two 3450kW steam turbine-driven alternators are installed, and there is also a diesel set with the same output. Steam is produced in two watertube boilers arranged to burn either oil fuel or boil-off gases.

TECHNICAL PARTICULARS

Length, oa	approx 283.00m
Length, bp	approx 270.00m
Breadth, moulded	43.40m
Depth, moulded	
to main (upper) deck	26.00m
to trunk deck	32.80m
Width of double skin	
side	2.53m
bottom	3.10m
Draught	
design	11.40m
summer	12.00m
scantling	12.40m
Gross	96,508gt
Displacement (design)	102,000tonnes
Lightweight	30,740tonnes
Deadweight	
design	71,450dwt
summer	77,450dwt
scantling	81,450dwt
Block coefficient (design)	0.745
Speed, service, 85% MCR, design draught	20.60knots
Cargo capacity	145,600m ³
Bunkers	
heavy oil	7,490m ³
diesel oil	440m ³
water ballast	57,000m ³
Fuel consumption, main engine	171.7/tonnes/day
Classification	American Bureau of Shipping, -A1, E, Liquefied Gas Carrier, Ship Type 2G (Membrane Tank, max pressure 25kPaG, min temp -163°C, SG 500kg/m ³), SH, SH-DLA, SHCM, SFA (40) +AMS, +ACCU, UWILD, PMS including CMS, NIBS, HM3+R with Descriptive Note: 'Slam Warning, Hull Girder Stress, Full VDM'
Percentage of high-tensile steel used in construction	approx 13%
Main engine	
Design	direct reversible steam turbine
Model	UA-400
Manufacturer	Kawasaki Heavy Industries
Number	1
Output	29,050kW
Main boilers	
Number	2

Type	Water tube
Manufacturer	Kawasaki Heavy Industries
Output	2 x 66tonnes/h
Gearbox	
Make	Kawasaki Heavy Industries
Type	double-reduction, articulated
Number	1
Output speed	90rev/min
Propeller	
Material	Nickel-aluminium-bronze
Designer/manufacturer	Samsung/Nakashima
Number	1
Pitch	Fixed
Diameter	8600mm
Speed	90rev/min
Steam-turbine driven alternators	
Number	2
Make/type	Mitsubishi/AT42CF-B
Output/speed	2 x 3450kW/1800rev/min
Diesel-driven alternator	
Number	1
Engine make/type	STX-MAN/8L32/40H
Type of fuel	MDO
Output/speed	3664kW/720rev/min
Alternator type	Nishishiba
Output/speed	3450kW/720rev/min
Cargo tanks	
Number	4 x IMO Type 2 membrane (GTT Mk 3 system)
Cargo pumps	
Number	8
Type	submerged electric
Make	Ebara
Capacity	8 x 1700m ³ /h
Custody transfer system	Saab Rosemount
Integrated automation system	Kongsberg Maritime
Complement	41 plus 6 Suez crew
Bow thruster	
Make	Kawasaki Heavy Industries
Number	1
Output	2500kW
Bridge control system	
Make	Kawasaki
Type	part of main turbine installation
Fire detection system	
Make	Consilium Marine
Type	CS 3000
Fire extinguishing system	
Engine/room	High-pressure CO ₂
Make	Unitor
Radars	
Number	2
Make	Kongsberg
Model	DB 1025
Integrated bridge system	
Make	Kongsberg
Model	SEAMAP 1021
Contract date	29 October 2003
Launch/float-out date	9 July 2005
Delivery date	15 April 2006



SERI BALHAF: Mitsubishi's first dual-fuel diesel-electric LNG tanker

Shipbuilder: **Mitsubishi Heavy Industries, Ltd. Nagasaki Shipyard & Machinery Works, Japan**
 Vessel's name: **Seri Balhaf**
 Hull No.: **2223**
 Owner/Operator: **MISC Berhad**
 Country: **Malaysia**
 Designer: **Mitsubishi Heavy Industries, Ltd.**
 Country: **Japan**
 Model test establishment used: **MHI Nagasaki R&D Center, Japan**
 Flag: **Malaysia**
 IMO number: **9331660**
 Total number of sister ships already completed (excluding ship presented): **Nil**
 Total number of sister ships still on order: **1**

Seri Balhaf is the largest Japanese-built LNG Tanker to feature the Gaz Transport & Technigaz membrane cargo containment system (GTT No.96E 2F) and electric propulsion motors with a Dual Fuel Engine (DFE) system. This results in improved fuel efficiency for the main propulsion system, supplemented by the high propulsive performance achieved by using a refined hull form developed using CFD (Computational Fluid Dynamics).

The principal dimensions of the membrane tanks were optimised taking into account the requirements of LNG terminals world-wide, with particular attention given to major Japanese, Korean and Taiwanese terminals. Cargo tank dimensions were determined to minimise sloshing dynamic loads.

The water ballast tanks adjacent to No.2 & 3 cargo tanks are divided into two pairs to facilitate safe ballast water exchange by the displacement method whilst remaining within the vessel's designed longitudinal strength parameters. The ballast exchange is automated by Mitsubishi Heavy Industries' ABE (Automatic Ballast Exchange) system.

One fuel gas pump of submerged type is provided in each of No.2 & 3 cargo tanks. Where natural boil-off is inadequate for vessel needs forced boil-off gas is supplied using cargo LNG transferred by fuel gas pump or spray pump from cargo tanks.

The propulsion plant consists of two electric propulsion motors and four Wärtsilä dual fuel engines (3 x 12V50DF plus 1 x 6L50DF). These dual fuel engines can run in MDO mode, burning diesel oil only, and in gas mode, burning mainly gas with diesel oil as a pilot fuel. In the gas mode the engines can use forced boil-off gas supplied as described above or natural boil-off gas generated in the cargo tanks. The natural boil-off gas is transferred to the engine room through a low duty gas compressor installed in the cargo machinery room.

The engines are arranged in two separate machinery spaces, each with independent fuel systems, seawater cooling systems, fresh water cooling systems, ventilation systems, and fire detection devices.

Two ABB AMZ 1120MS08 LSF electric propulsion motors drive one propeller through a Renk NDSH-3920 reduction gear. Each electric propulsion motor has independent feeder circuits and is operated individually. A gas combustion unit in the engine casing burns surplus boil-off gas where the amount of natural boil-off gas exceeds vessel requirements.

A Mitsubishi Heavy Industries DCS (Distributed control system) is provided to facilitate monitoring and control of the principal machinery and the equipment in the engine and cargo handling areas from the centralised control room.

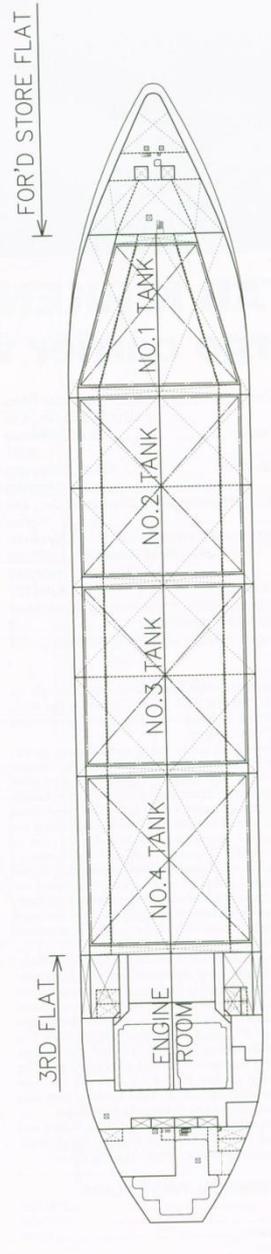
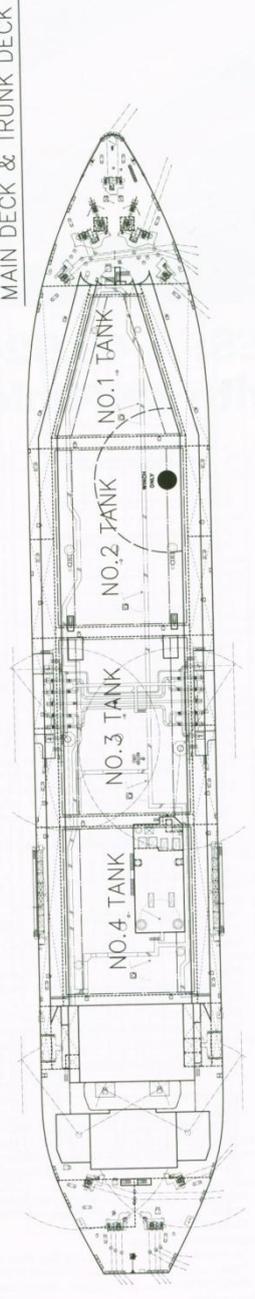
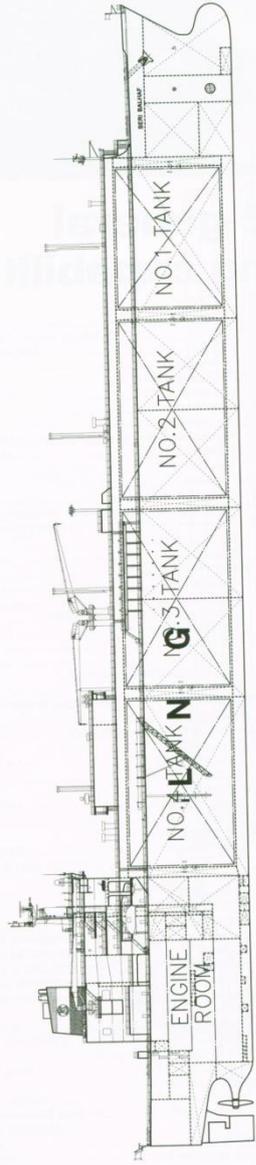
Seri Balhaf and her sister ship, *Seri Balgis*, have been chartered to lift Yemen LNG cargoes for 20 years, plus further options.

TECHNICAL PARTICULARS

Length oa: 294.6m
 Length bp: 281.6m
 Breadth moulded: 46.5 m
 Depth moulded to upper deck: 25.8 m
 Width of double skin:
 side: 2.36m approx.
 bottom: 3/1m approx.
 Draught:
 scantling: 12.40m
 design: 11.15m
 Gross: 107,633gt
 Deadweight, scantling: 91,201dwt
 Speed, service: 19.5knots at 100% MCR
 Cargo capacity:
 Liquid volume: 157,720m³
 (100% at -163 degrees C)
 Bunkers:
 Diesel oil: 2600m³
 Water ballast: 57,900 m³
 Daily fuel consumption:
 Main engine only: 129tonnes/day
 Classification society and notations: Bureau Veritas I,
 +Hull, +Mach Liquefied Gas Carrier/
 LNG, +Unrestricted navigation, +AUT-UMS,
 +VeriStar-Hull, Mon-Shaft, Inwatersurvey
 Main generator engines:
 Design & manufacturer: Wärtsilä
 Model: 12V50DF and 6L50DF
 Number: 3 x 12V50DF + 1 x 6L50DF
 Type of fuel: MDO and Natural Gas
 Output of each engine: 3 x 11,400kW
 + 1 x 5700kW
 Propulsion Electric Motor:
 Design & manufacturer: ABB
 Number & model: 2 x AMZ 1120MS08 LSF
 Gearbox:
 Make: Renk
 Number & model: 1 x NDSH-3920
 Output: 24,750kW x 78.0rev/min

Propeller:
 Material: Nickel aluminum bronze
 Designer/Manufacturer: Mitsubishi Heavy Industries, Ltd.
 Fixed/Controllable pitch: 1 x Fixed
 Diameter: 9.0m
 Speed: 78.0rev/min
 Exhaust-gas scrubbing equipment:
 Manufacturer: Aalborg Industries K.K.
 Type: Mono-pressure, forced circulation, fin tube type
 Boiler:
 Number & type: 1 x Cylindrical type
 Make: Aalborg Industries K.K.
 Output, each boiler: 9000kg/h
 Mooring equipment:
 Number: 2 x mooring winch/windlass,
 7 x Mooring winch
 Make: Friedrich Kocks GmbH
 Type: Electro-hydraulic
 Special lifesaving equipment:
 Number of each and capacity: 2 x 44 persons
 Make: Hyundai Life boats Co., Ltd.
 Type: FRP enclosed type lifeboat
 Cargo tanks:
 Number: 4
 Grades of cargo carried: LNG
 Cargo pumps:
 Number: 8
 Type: Electric motor driven centrifugal submerged
 Make: Ebara Corporation
 Capacity (each): 1850m³/h / 170tonnes/h
 Cargo control system:
 Make: Mitsubishi Heavy Industries, Ltd.
 Type: Distributed Control System
 Ballast control system:
 Make: Mitsubishi Heavy Industries, Ltd.
 Type: Automatic Ballast Exchange system
 Complement:
 Officers: 12
 Crew: 19
 Supernumeraries/Spare: 5
 Suez/Repair Crew: 4
 Bow thrusters:
 Make: Kawasaki Heavy Industries, Ltd.
 Number & output: 1 x 2000kW
 Fire detection system:
 Make: Autronica A/S
 Fire extinguishing systems:
 Cargo holds: Dry powder
 Engine room: CO₂
 Radars:
 Number & make: 2 x Japan Radio Co., Ltd.
 Models: 1 x X-band with ARPA,
 1 x S-band with ARPA
 Integrated bridge:
 Make: Japan Radio Co., Ltd.
 Waste disposal plant
 Incinerator: Sunflame Co., Ltd.
 Sewage plant: Taiko Kikai Industries Co., Ltd.
 Contract date: 23 July 2004
 Launch/float-out date: 16 February 2008
 Delivery date: 1 January 2009

SERI BALHAF





**CARACTERÍSTICAS
PRINCIPALES
MAIN PARTICULARS**

GENERALIDADES

El buque ha sido proyectado para transportar en sus cuatro tanques, convenientemente aislados, de doble membrana, 138.000 m³ de LNG a -163° C, con un peso específico de 0,46, y suficientes consumos para unas 20.000 millas navegando a 19,5 nudos al 90% de la PMC del equipo propulsor.

Ha sido diseñado, en principio, para efectuar tareas de carga en las terminales especializadas de Ras Laffan (Qatar), DAS Island (EAU), Port Fortin (Trinidad y Tobago), Bethonia (Argelia), Bonny (Nigeria), y West Shelf (Australia), y descargar en las terminales de Huelva (España) y Boston (USA). Está preparado asimismo para cumplir los requisitos presentes y futuros de las terminales de descarga en Barcelona, Bilbao y Cartagena, así como en la terminal de Peñuelas, en Puerto Rico. El tiempo de descarga de todo su cargamento de LNG es de unas 12 horas.

Las formas del casco, así como todo el sistema de propulsión y los sistemas de generación eléctrica, han sido diseñados para una máxima eficiencia energética.

Esloza total / Length o.a.	284,4 m.
Esloza entre pp / Length b.p.	271,0 m.
Manga de trazado	42,5 m.
Moulded Breadth	
Puntal a Cbta. Principal	25,4 m
Depth to Main Deck	
Puntal a Cbta. Tronco	32,2 m
Depth to Trunk Deck	
Calado de diseño	11,4 m
Design Draught	
Calado de escantillonado	12,3 m.
Scantling Draught	
Peso muerto	68.200 t
Deadweight	
Capacidad de carga (100%)	138.000 m ³
Cargo Capacity (100%)	
Sistema de contención de carga	Membrana NO96 © GTT
Cargo Containment system	
Capacidad de lastre	49.600 m ³
Ballast capacity	
Potencia propulsora	28.000 kW a 83 rpm
Propulsion Power	
Velocidad de servicio	19,5 nudos
Service Speed	knots
Autonomía / Range	20.000 m.n.
Tripulación / Crew	34 personas
Clasificación	Lloyd's Register of Shipping
Classification	≈100 A1, Liquefied Gas Tanker, Ship type 2G*, Methane in Membrane tanks, Max. pressure 0,25 bar, Min. temperature -163° C, Shipright (SDA), *IWS, LI, ≈ LMC, UMS, CCS, PORT, NAV 1, IBS. With the Descriptive Notes: Shipright FDA, TGM, CM, SCM, ES (≈2)

GENERAL

The Sestao Knutsen is, as mentioned earlier, specially designed to carry, in four membrane tanks, 138,000 m³ (total capacity, excluding the dome, internal structure and fittings) of liquefied natural gas of a specific gravity of 0.46, at -163° C, with sufficient fuel capacity for a 20,000-mile range navigating at 19.5 knots at 90% of MCR of the propulsion engine.

The ship is arranged with a flush deck, raked stern and bulbous bow without a forecastle. The accommodation, including the bridge and propulsion machinery are located aft. The General Arrangement can be seen in the drawing that accompanies this description.

The propulsion power is provided by a steam turbine driving a single shaftline, fitted with a fixed-pitch propeller. The main particulars, capacities, class and additional notations are indicated in the box on this page.

It is designed initially to load at the dedicated terminals of Ras Laffan (Qatar), Das Island (United Arab Emirates), Port Fortin (Trinidad y Tobago), Bethonia (Algeria), Bomny (Nigeria) and West Shelf (Australia).



SK SUMMIT: Daewoo's KOGAS contribution

Shipbuilder: Daewoo Heavy Industries Ltd, Korea
 Vessel's name: SK Summit
 Hull number: 2202
 Owner/operator: Omnia Enterprises SA, Panama/SK Shipping Co Ltd, Korea
 Designer: Daewoo Heavy Industries Ltd, Korea
 Flag: Panama
 Total number of sister ships already delivered: -
 Total number of sister ships still on order: 2

SK Summit is another vessel built for KOGAS (Korea Gas Corp) charter and represents Daewoo's interpretation of that company's requirements. The yard has produced a design with principal dimensions only marginally different from Hanjin Muscat (qc), and which is similarly powered by steam turbines; these, despite their high fuel consumption, have proved to be a successful prime mover for LNG carriers. This is because of their ability to use boil-off gases from the cargo in their boilers, as well as fuel oil. However, Daewoo has selected Kawasaki, rather than Mitsubishi, to supply the UA-400 type, slightly higher powered and faster running (40,000shp/96rev/min) turbine set for its vessel.

With a supply of steam readily available, two 3450kW turbo-alternators are the main source of electrical power, supplemented by a supply from a similar sized diesel-driven set. The demand for more economic and safer seaborne transportation of LNG has resulted in the development of integrated automation systems for both cargo and engine room machinery in most vessels of this type. That fitted to SK Summit has been designed and programmed by Yamatake-Honeywell using the TDC 3000 LCN system, with control and monitoring carried out from a centralised administration and control centre (CACC) located in the accommodation block.

Daewoo's commitment to the building of LNG carriers is evidenced by its involvement at all stages of the construction process and high level of quality control,

required for the insulation boxes, cargo pipes and pump towers, and the Invar sheets used in the tank insulation. Over 125km of welding was needed to join this nickel-alloy steel, which has a very small thermal shrinkage coefficient at very low temperatures, and Daewoo developed its own technology, plus an automatic welding machine, to carry out this work.

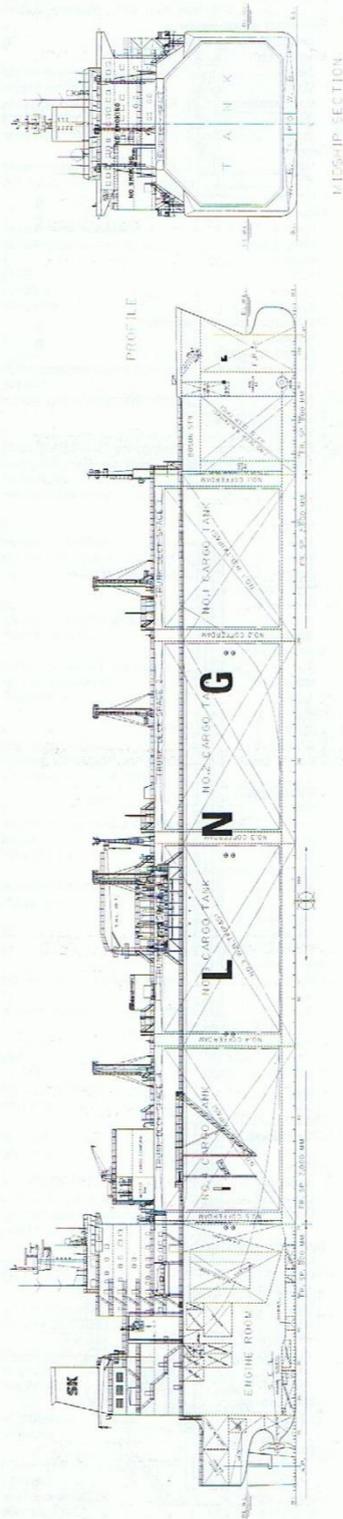
The company also built three, state-of-the-art fabrication shops at Okpo Shipyard, especially to manufacture the many components of an LNG installation, and developed the first LNG carrier simulator, which allows designers and operators the opportunity to carry out realistic ship operations by computer. The cargo containment system adopted for SK Summit is a No 96 E-2 design from Gaz Transport & Technigaz (GTT), which uses the same principles as the 96-2 membrane system adopted for Hanjin Muscat, namely primary and secondary membranes of 0.70mm Invar sheets in conjunction with expanded perlite beads contained in plywood boxes, to give a total thickness of 530mm.

PRINCIPAL PARTICULARS

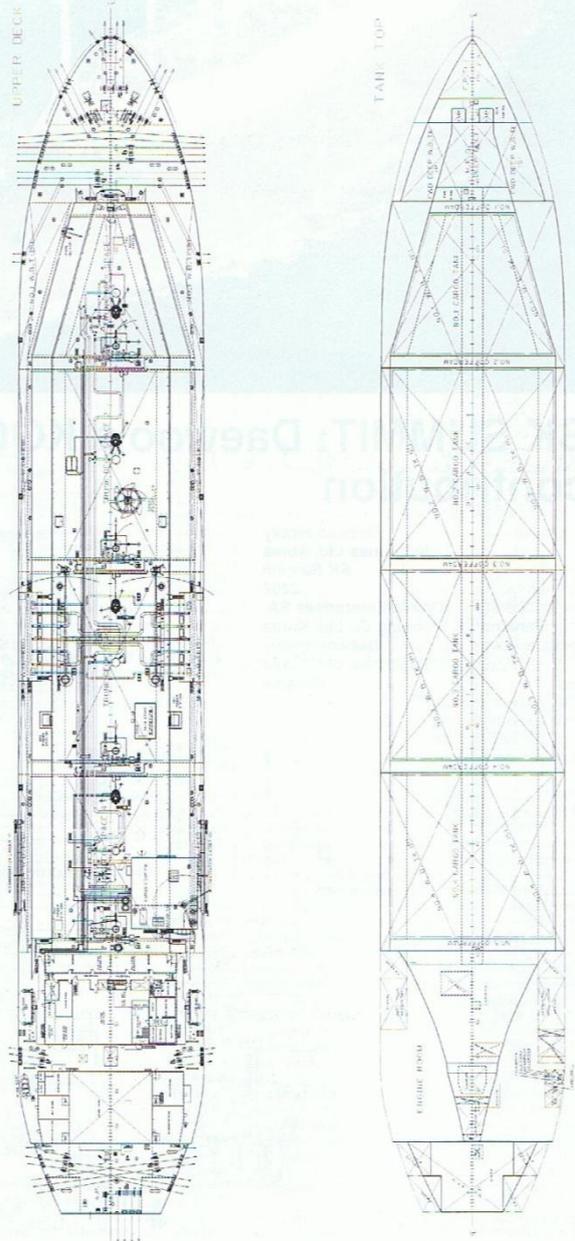
Length, oa 277.00m
 Length, bp 266.00m
 Breadth, moulded 43.40m
 Depth, moulded to main deck 26.00m
 Gross 95,400gt
 Deadweight, design 69,000dwt
 scantling 76,000dwt
 Draught, design 11.30m
 scantling 12.00m
 Speed, service, with 21% sea margin 20.30knots
 Cargo capacity
 100% at -163°C 138,000m³
 Bunkers
 heavy fuel 6,000m³
 diesel oil 470m³
 Water ballast 52,000m³
 Fuel consumption, main engine only 203tonnes/day
 Classification Korean Register of Shipping +KRS1
 Liquefied Natural Gas Carrier, 2G3M(R), -163°C,
 .05SG(1GC), +KRM1-UMA 1WS, and Det Norske Veritas,
 1A1, Tanker for LNG, EO, LCS(SID), W1-OC,

..... Ship Type 2G (-163°C, 500kg/np, 0.2bar)
 Percentage of high-tensile steel used in construction Nil
 Main engine
 Design Kawasaki Heavy Industries Ltd
 Model UA-400 steam turbine
 Manufacturer Kawasaki Heavy Industries Ltd
 Number 1
 Output 40,000shp/96rev/min
 Gearbox
 Make Kawasaki Heavy Industries Ltd
 Model UA-400
 Number 1
 Propeller
 Material Nickel-aluminium-bronze
 Manufacturer Hyundai Heavy Industries Ltd
 Number 1
 Pitch Fixed
 Diameter 8200mm
 Speed 96rev/min
 Steam turbine-driven alternators
 Number 2
 Turbine make/type -
 Alternator make/type Hyundai Heavy Industries/HFJ5
 714-44E
 Output 2 x 3450kW/1800rev/min
 Diesel-driven alternator
 Number 1
 Engine make/type Ssangyong-MAN B&W/8L32/40
 Alternator make/type Hyundai Heavy Industries/HFJ5 804-1
 Output 3450kW/720rev/min
 Boilers
 Number 2
 Type UME 68/59 double-drum
 Make Kawasaki Heavy Industries Ltd
 Output 2 x 68,000(max), 58,000(min)kg/h
 Hose-handling cranes
 Number 2
 Make/type Nor-Marine/MCV1800-10-24Ex
 Capacity/speed 10tonne/24m/min
 Mooring equipment
 Number 2 x windlass; 8 x mooring winch
 Make Brissonneau et Lotz
 Type Electro-hydraulic
 Cargo tanks
 Number 4
 Product range Liquefied natural gas
 Coated tanks Gaz Transport cargo containment system with Invar membrane
 Cargo pumps
 Number 8
 Type 8 x 12EC-24 submerged centrifugal
 Make Ebara
 Capacity 8 x 1700m³/h
 Cargo/ballast control system
 Make Yamatake Industrial Systems
 Type TDCS-3000LCN
 Complement
 Officers 26
 Crew 14
 Bow thruster
 Make Kawasaki Heavy Industries Ltd
 Number 1
 Output 2000kW/210rev/min
 Bridge control system
 Make -
 One man operation Yes
 Fire detection system
 Make Nittan System AB
 Type NSAC-1 addressable type
 Fire extinguishing system
 Engine room Fixed CO₂
 Make Namyang
 Radars
 Number 3
 Make Kongsberg Norcontrol
 Models Databridge 2000BL
 2 x S-band; 1 x X-band
 Satellite navigation system
 Make Trimble
 Model NT 200D
 Integrated navigation system
 Make Kongsberg Norcontrol
 Model DB2000BL/AP2000
 Waste disposal plant
 Incinerator
 Make Kangrim
 Model UW1-350MP
 Waste compactor
 Make Metos Co
 Model Uson 8251
 Sewage plant
 Make Jonghap Machine Co
 Model Aerob-25
 Contract date 23 December 1996
 Launch/float-out date 4 April 1998
 Delivery date 3 August 1999

SK SUMMIT



94



SIGNIFICANT SHIPS OF 1995



TRINITY ARROW: Imabari Group delivers its first LNG carrier

Shipbuilder:.....**Imabari Shipbuilding Co Ltd (Koyo Dockyard), Japan**
 Vessel's name:.....**Trinity Arrow**
 Hull number:.....**2258**
 IMO number:.....**9319404**
 Owner/operator:.....**Cypress Maritime (Panama SA, Panama/K Line LNG Shipping UK Ltd, UK)**
 Designer:.....**Imabari Group (Koyo Dockyard), Japan**
 Model test establishment used:.....**Shipbuilding Research Centre of Japan, Japan**
 Flag:.....**Panama**
 Total number of sister ships already completed:.....**Nil**
 Total number of sister ships still on order:.....**2**

IMABARI Shipbuilding Group's first LNG tanker is understood to be the largest capacity vessel of this type yet built in Japan. Although conforming to the traditional 'membrane-type' gas tanker layout with four cargo spaces, each containing an independent trapezoidal cargo tank which extends into a trunk above the upper deck, the design is unusual: in a departure from the norm, No 1 tank is of horizontally trapezoidal shape. It is claimed that this is the first time the arrangement has been used, and that it brings benefits of increased cargo capacity and, by virtue of its shape, allows an improved hull form to be developed, leading to better propulsive performance and reduced fuel consumption.

Because *Trinity Arrow* is intended for worldwide trading rather than long term operation on a specific route, Imabari sought to ensure compatibility with most major LNG terminals in its design. This features a complete double-hull structure with cargo tank divisional bulkheads forming cofferdams heated by circulating glycol water to keep the temperature above +5°C, to suit the physical properties of the steel, in accordance with the IGC code.

A GTT Mk III cargo containment system has been adopted. This has a primary barrier of 1.2mm SUS membrane with orthogonal corrugations, and a secondary barrier of Triplex membrane, sandwiched between first and second glass fibre reinforced polyurethane foam layers. The insulation has a total thickness of 270mm, which allows an LNG boil off less than 0.15% each day to be maintained during a voyage.

Each cargo tank is fitted with two 1700m³/h Shinko submerged cargo pumps, and one 50m³/h cargo stripping/spray pump. A further cargo pump of 550m³/h is provided for emergency use. Cargo control is carried out from the bridge, allowing full observation and monitoring of all operations, which are handled through port and starboard, midship manifolds. An automatic ballast exchange system is installed for use at sea, taking into consideration the strength, stability and safety aspects of the procedure, in accordance with IMO requirement A868(20). As is the current trend, separate bunker tanks are provided for holding low-sulphur fuel,

for use in sulphur emission control areas (SECAs).

Trinity Arrow is fitted with a Kawasaki UA-400 turbine, supplied with steam from two water tube boilers arranged to burn heavy oil and boil-off gas. This installation develops a maximum continuous rating of 29,420kW at 81rev/min, and drives a fixed pitch propeller through a double-reduction, tandem articulated gearbox integrated with the main turbine, for a service speed of 19.5knots when running at 80% full power. Three Nishishiba 3250kW alternators are fitted, two driven by Shinko steam turbine prime movers, and one connected to a Yanmar diesel engine, to satisfy electrical requirements.

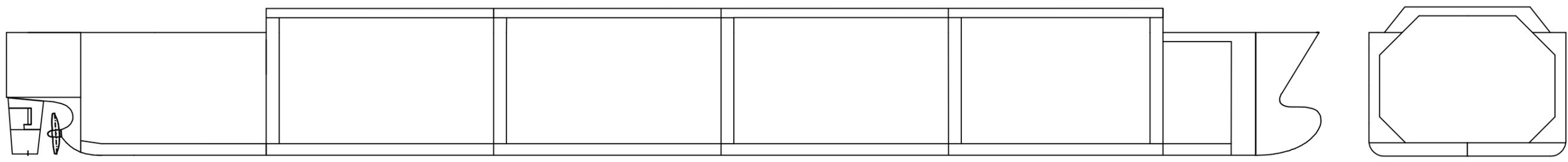
TECHNICAL PARTICULARS

Length, oa.....289.00m
 Length, bp.....276.00m
 Breadth, moulded.....44.70m
 Depth, moulded.....33.12m
 to trunk deck.....26.00m
 Width of double skin.....2.51m
 side.....3.20m
 bottom.....11.37m
 Draught.....12.60m
 design.....101.080gt
 scantling.....72.318dwt
 design.....85.511dwt
 Gross.....19.50knots
 Deadweight.....154,982m³
 heavy oil.....6460m³
 diesel oil.....700m³
 water ballast.....56,780m³
 Fuel consumption.....161tonnes/day
 Classification.....Lloyd's Register +100A1, Liquefied Gas Tanker, Ship Type 2G, Membrane (LNG) in Membrane Tanks, Max Vapour Pressure 0.25bar, Minimum Temperature -163°C, ShipRight (SDA, FDA plus CM), *IWS, L1, +LMC, UMS, NAV 1, IBS, ICC
 Percentage of high tensile steel used in construction.....10.30%
 Percentage of stainless steel used.....0.10%
 Main engine.....Direct reversible steam turbine
 Manufacturer.....Kawasaki Heavy Industries
 Model.....UA-400
 Number.....1
 Output, MCR.....29,420kW/81rev/min
 Output, NCR.....26,480kW/78.2rev/min
 Main boilers.....2
 Number.....2
 Manufacturer.....Kawasaki Heavy Industries
 Type.....UME LL153 watertube
 Output, max.....2 x 66,000kwh
 Gearbox.....2
 Type.....Tandem, articulated, double reduction, integrated with main turbine

Propeller.....Nickel-aluminium-bronze
 Designer/manufacturer.....Mitsubishi Heavy Industries
 Number.....1
 Pitch.....Fixed
 Diameter.....8800mm
 Steam turbine-driven alternators.....2
 Number.....2
 Turbine manufacturer.....Shinko
 Alternator make.....Nishishiba
 Output/speed.....2 x 3250kW/1800rev/min
 Diesel-driven alternator.....1
 Number.....1
 Engine make.....Yanmar
 Type of fuel used.....Diesel/marine gas oil
 Output/speed.....3404kW/720rev/min
 Alternator make.....Nishishiba
 Output/speed.....3250kW/720rev/min
 Cargo tanks.....4 x IMO type 2G membrane type, GTT Mk III system
 Cargo pumps.....8
 Number.....8
 Type.....vertical submerged
 Make.....Shinko
 Capacity.....8 x 1700m³/h
 Ballast/cargo control systems.....Kokogawa
 Make.....Kokogawa
 Type.....Integrated automation system
 Complement.....11
 Officers.....18
 Crew.....6
 Supernumeraries.....6
 Suez crew.....6
 Bow thruster.....Kawasaki Heavy Industries
 Make.....Kawasaki Heavy Industries
 Number.....1
 Output.....2200kW
 Bridge control system.....Japan Radio Co
 Make.....Japan Radio Co
 Type.....Integrated automation system
 One man operation.....Yes
 Fire detection system.....Nippon Nahyco
 Make.....Nippon Nahyco
 Type.....FF-1515-4
 Fire extinguishing system.....Unitor, dry powder
 Cargo area (deck).....Unitor, dry powder
 Engine room.....Kashiwa, high expansion foam
 Radars.....2
 Number.....2
 Types.....1 x JMA-922M9XA, LY-band
 1 x JMA-932M5A, S-band
 Make.....Japan Radio Co
 Integrated bridge system.....Japan Radio Co
 Make.....Japan Radio Co
 Waste disposal plant.....Sunflame DSV 600 SA1
 Incinerator.....Sunflame DSV 600 SA1
 Waste compactor.....Electrolux
 Sewage plant.....Taiko Kikai SPT-65
 Contract date.....3 August 2004
 Launch/float-out date.....17 August 2006
 Delivery date.....31 March 2008

ANEXO III

Croquis conceptual buque proyecto



1 2 3 4 5 6 7 8 9 10 11 12

A B C D E F G H

A B C D E F G H

1 2 3 4 5 6 7 8 9 10 11 12

 UNIVERSIDADE DA CORUÑA	PROYECTO: 15 105 P
ESCOLA POLITÉCNICA SUPERIOR	
CROQUIS DISPOSICIÓN GENERAL	
AUTOR: ISMAEL GRANDAL MOURIZ	ESCALA 1:900